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2 **On the stability and phase behavior of Titan's subsurface liquid col-**  
3 **umns**

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7 **ABSTRACT**

8 On Titan, liquid hydrocarbon may stay in the subsurface porous permeable crust known as the  
9 alkanofers, analogous to water in Earth's aquifer. In addition to pressure gradient, the subsurface  
10 liquid in alkanofers is subject to vertical compositional grading due to the gravity and tempera-  
11 ture gradient. The common wisdom is that the liquid would normally stay underground in a sta-  
12 bility established by the pressure that increases with depth as observed in aquifers on Earth.  
13 However, Titan's liquids consist of nitrogen and hydrocarbons, mainly methane and ethane, the  
14 behavior of which is very sensitive to temperature and pressure. Consequently, the liquid density  
15 does not always increase with depth, thus may introduce a reverse density profile that leads to  
16 vertical convective instability of the liquid column. If reverse density profiles are present, capil-  
17 lary pressures arising from liquid trapped within small pores in the crust can help with the col-  
18 umn stability. The liquid held in the capillaries can seal the space below it thus helping with the  
19 stability, unless the overpressure built from underneath becomes larger than the capillary pres-  
20 sure, which causes leakage to allow the liquids to seep upward from the deep. This situation is  
21 analogous to hydrocarbon seeps on Earth, where oil and natural gas escape the reservoir and flow  
22 slowly through network of cracks to the surface. An algorithm based on an extended Gibbs equa-

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23      tion commonly used in petroleum reservoir engineering is employed in this work to produce  
24      pressure, density, and compositional profiles for evaluating the stability and phase behavior of  
25      Titan's subsurface fluids.

26

27 KEYWORDS: Titan; subsurface liquid; alcanofer; thermo-gravitational effects; capillary pres-  
28 sure

29

30 **1. Introduction**

31 In gravitational fields, any fluid mixtures will experience the hydrostatic effect and com-  
32 positional grading with depth, which provide vertical compositional gradient with a tendency of  
33 heavy components migrating to greater depths. In the meantime, the temperature gradient due to  
34 geothermal activities introduces an opposing effect to the composition, because the lighter com-  
35 ponents also tend to go deeper through diffusion as the temperature increases. These thermo-  
36 gravitational effects are very important, e.g., in oil-gas recovery from reservoirs on Earth (Høier  
37 & Whitson, 2000; Galliero et al., 2016), where the composition of hydrocarbon at the well bore  
38 is different from the composition in the reservoir.

39 Similar situations would likely occur in the subsurface alkanofers on Titan (Vance et al.,  
40 2012; Mousis et al., 2014) where the hydrocarbon liquids may attain high hydrostatic pressures  
41 due to the depth, as well as higher temperatures due to the temperature gradient. The subsurface  
42 alkanology, analogous to terrestrial hydrology, may exist with water-ice upper crust that is ther-  
43 mally conductive and likely porous and has fractures to allow subsurface liquid flow. Methane-  
44 based hydrological cycle on Titan is discussed in a comprehensive review paper (Hayes et al.,  
45 2018). The topmost layer of the crust may also be covered by methane clathrate of several kilo-  
46 meters thick that increases the temperature gradient below it due to its lower heat conductivity  
47 than water ice (Kalousova & Sotin, 2020). The existence of clathrate crust could in fact be the  
48 most realistic crust environment on Titan due to the presence of hydrocarbon.

49 While the hydrostatic pressure on Earth is easily calculated for water based on its density  
50 behavior with temperature and pressure, it is not the case with Titan's liquid, which is a mixture  
51 of nitrogen and hydrocarbons (Tan et al., 2013; 2015) – mainly methane and ethane (Brown et  
52 al., 2008; Mastrogiuseppe et al. 2015; Tan & Kargel, 2018). On the surface, the liquid is in equi-

53 librium with the atmosphere at conditions observed by Huygens probe. At this equilibrium, the  
54 density of the mixture, thus also the composition, is sensitive to pressure and temperature in a  
55 counter-intuitive way, where it can become denser with temperature and lighter with pressure  
56 (Tan et al., 2015).

57 Recent treatments have simultaneously applied both gravitational and thermal diffusion  
58 to obtain the compositional grading so that the subsurface conditions, including the pressure gra-  
59 dient, can be calculated more realistically for Titan's alkanofers (Tan & Kargel, 2020; Cordier et  
60 al., 2021). The treatments assume that the subsurface liquid column has reached a steady state, so  
61 that stationary compositional gradients can be obtained. In fact, this is generally true for hydro-  
62 carbon reservoir on Earth, where the liquid column is stable as the vertical convective flow is  
63 practically absent (England et al., 1987). As this work will show later, it is not always the case  
64 for Titan's subsurface liquids, of which the density profile can be reversed, i.e., the density de-  
65 creases with depth. This reverse density profile leads to convection, thus unstable system (Gal-  
66 liero et al., 2016). Therefore, it is very critical to evaluate the stability of liquid columns on Ti-  
67 tan, which is usually taken for granted despite its importance for more realistic conditions of the  
68 subsurface liquids.

69 As happens on Earth, subsurface liquids, both water and hydrocarbons, may also be  
70 stored inside small pores underground. Liquids trapped in pores have strong interaction with the  
71 pore wall, known as capillary pressure, which hold the liquids from expulsion (Berg, 1975). Only  
72 if there is a sufficient pressure difference across the ends of the pores, the capillary pressure is  
73 overcome to release the liquids out from the pores. Therefore, a layer of crust with small pores  
74 can entrap liquids and withstand pressure difference that is less than the existing capillary pres-  
75 sure to block any possible flow across the layer (England et al., 1987). These filled capillaries

76 effectively seal the space below them, such as that in aquitard or caprock on Earth sealing oil  
77 reservoirs at the top, and thus stabilize the liquid columns, e.g., from vertical convective flow as  
78 mentioned earlier. Such a layer may be called as alkanotard on Titan as the liquid contains most-  
79 ly alkanes, i.e., methane and ethane in this work. The capillary pressure is stronger in smaller  
80 pores, thus deeper location due to compaction. Though the exact magnitude of the capillary pres-  
81 sure that helps the column stability is not possible to obtain, even on Earth due to a vast number  
82 of factors, the order of magnitude can be estimated using a state-of-the-art approach applied in  
83 this work. Capillary uptake into crust with nanometer-size pores on Titan was first studied using  
84 conventional Kelvin's equation (Voss et al., 2007), which treats the vapor phase as an ideal gas  
85 and the liquid phase is assumed to be incompressible, both of which are not valid for Titan's flu-  
86 ids as explained later. Moreover, the capillary pressure was not discussed in that paper.

87 In this work, several cases with thermo-gravitational effects are considered for Titan's  
88 subsurface liquids, which are adequately modeled as ternary mixtures of nitrogen, methane, and  
89 ethane (Tan & Kargel, 2018). For a single fluid phase, liquid in this case, the thermo-  
90 gravitational effects are readily calculated using a simple algorithm (Galliero et al., 2017) as  
91 done before (Tan & Kargel, 2020). The algorithm allows us to simultaneously obtain pressure  
92 and compositional gradients, and consequently the density profile, for a liquid mixture subject to  
93 gravity and a temperature gradient in convection-free conditions. For the record, the subroutine  
94 applying this algorithm is not specific to a certain equation of state (EOS), so that any EOS can  
95 be used with it to do the calculations if the inputs required by the subroutine are provided. We  
96 use PC-SAFT EOS (Gross & Sadowski, 2001), which is accurate in describing fluid phases of  
97 mixtures, to be coupled with the subroutines for our investigation. A similar thermo-gravitational  
98 treatment has been done with this ternary mixture by Cordier et al. (2021), in which the same

99 EOS was used but with a different binary parameter, as well as different thermo-diffusion ap-  
100 proach, compositions on the surface, and crust environments. Nevertheless, as shown later, our  
101 work applies better binary parameter, thermo-diffusion approach, and surface compositions at  
102 low- and high-latitude regions, for water-ice and methane-clathrate crusts. Importantly, we inves-  
103 tigate the stability of the subsurface liquids, which has never been done before. The stability  
104 analysis, as also shown later, is based on the density profile.

105 Upon evaluation on the vertical stability of liquid columns under various temperature  
106 gradients, which are given in Appendix A, the corresponding profiles of capillary pressure will  
107 also be determined with respect to depth. This way, when a reverse density profile is present, the  
108 magnitude of capillary pressure at the depth of interest that helps with the stability can also be  
109 estimated. Note that the evaluation in this work is only based on thermodynamic steady states, so  
110 that any implications leading to temporal variations and fluid dynamics in the liquid columns and  
111 changes of properties in the crust are not considered, thus open for further investigations.

112 This paper starts with revisiting the analogy between alkanofers on Titan with aquifers on  
113 Earth, which discloses some differences to be cautioned. The methods of thermo-gravity and ca-  
114 pillary-pressure calculations are then briefly discussed, followed by the results and discussion.  
115 The paper ends with conclusions and remarks as well as appendices that include the algorithms  
116 of the thermo-gravitational effects. A supplementary material is also given to accompany the pa-  
117 per in presenting the numerical results plotted in the figures as well as the subroutines coded in  
118 FORTRAN for the thermo-gravitational effects.

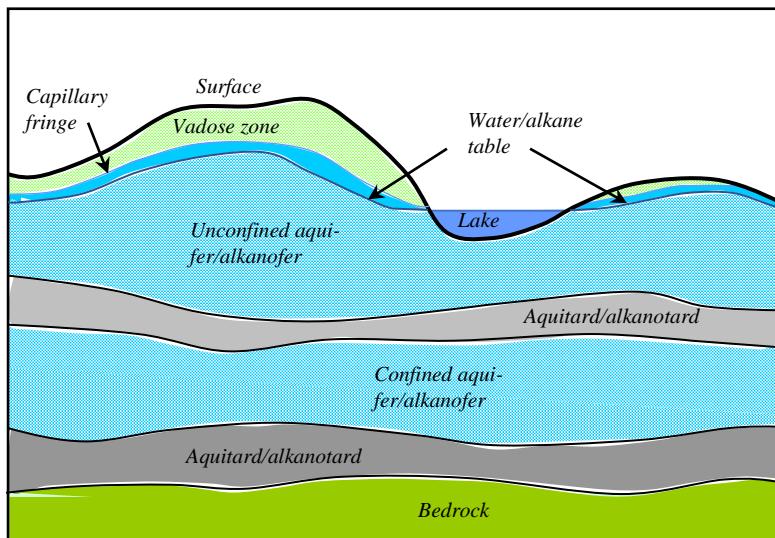
119 **2. Analogy: Titan's alkanofers and Earth's aquifers**

120 It may be beneficial to consider the analogy between alkanofers on Titan with aquifers on  
121 Earth in more details, which can be summarized and illustrated in Fig. 1. On Earth, starting from

122 the surface, the atmospheric air may penetrate the vadose zone where liquid does not occupy the  
123 whole space. In this zone the pressure is the same as the atmospheric pressure down to the so-  
124 called water table, which usually has a profile roughly following the surface curvature except in  
125 open liquid bodies such as lakes where the profile is horizontally flat. On Titan, it would be  
126 called the alkane table, just to borrow the term from Earth's case. Below the table, there is an  
127 unconfined aquifer, or unconfined alkanofe on Titan, where the hydrostatic pressure takes place  
128 in constant communication with the atmosphere through the vadose zone. Therefore, the highest  
129 level that can be reached by liquids in this layer is the table. At the bottom of the unconfined aq-  
130 uifer, there is an aquitard, i.e., a layer barely permeable to water (Freeze & Cherry, 1975), which  
131 may trap another deeper aquifer in the so-called confined aquifer. By analogy, an equivalent al-  
132 kanotard may be assumed to exist on Titan. In the confined zone, the liquid has both hydrostatic  
133 and lithospheric pressures. The latter may be caused by the full weight of the overlying crust ma-  
134 terials or just a part of the weight due to partial support from the crustal structure. This litho-  
135 spheric pressure can send the liquid from the confined aquifer to some height in the air, e.g., in  
136 an artesian well. Finally, the confined zone sits on another aquitard, or alkanotard on Titan,  
137 which seals the bedrock that may still contain some liquids.

138 While in many aspects the analogy seems to be comprehensive by substituting liquid wa-  
139 ter with alkane-rich liquids, as well as the silicate-rich crust with water-ice crust, there are im-  
140 portant differences outlined below. On Earth, we may have another fluid in addition to water,  
141 which is the hydrocarbons that we call oil and natural gas, so that we often encounter three-phase  
142 fluid system underground near hydrocarbon reservoirs. They are aqueous phase, oil (liquid)  
143 phase, and gas phase. On the other hand, Titan's fluid will not encounter liquid water until about  
144 100 kilometers under the surface due to the very low temperatures on the surface (Kalousova &

145 Sotin, 2020). Moreover, interaction between the fluid and water-ice crust result in clathrate hy-  
 146 drate phase in the top few kilometers near the surface (Kalousova & Sotin, 2020), which can also  
 147 be porous (Genov et al., 2004). The fluids as liquids will migrate until they are contained by al-  
 148 kanotards, which can simply consist of water-ice or clathrate crust with pores that are fully filled  
 149 with the liquid. Liquids confined in small pores are held tightly by capillary pressure so that ef-  
 150 fectively block any possible flow across them, unless there is an overpressure from outside the  
 151 pores. Importantly, there is only a single type of subsurface fluid on Titan, i.e., mixtures of nitro-  
 152 gen and alkanes. The fluid can be in vapor phase only in the vadose zone as the atmosphere pen-  
 153 etrates the top crust, but mostly liquid phase in other zones, unless the temperature and pressure  
 154 are high enough for the fluids to reach supercritical state or vapor-liquid equilibrium as shown  
 155 later.



156 **Fig. 1.** Analogy of Earth's aquifers and Titan's alkanofers: for Titan, water is replaced with al-  
 157 kane-rich liquid and aquifer/aquitard with alkanofer/alkanotard.

158 The presence of small pores in crusts makes the porous space available for storing liq-  
 159 uids. While the capillaries in Earth's crust may be occupied by both water and hydrocarbons,  
 160 which make the situation more complicated, those on Titan are occupied by the nitrogen-alkane

161 liquids only. Therefore, the overpressure across the capillaries, which may be provided by the  
162 buoyancy due to density difference of hydrocarbon and liquid water on Earth, e.g., in the hydro-  
163 carbon migration (England et al., 1987), must be given by the fluid itself on Titan, in addition to  
164 the full or partial weight of the overlying crusts if the liquid is in the confined zone. In this sense,  
165 Titan's fluids are analogous to both oils in Earth's hydrocarbon reservoirs and water in aquifers.  
166 They are made of a single kind of fluid mixture, but with different compositions depending on  
167 the location, depth- and latitude-wise according to the vertical temperature gradient and the tem-  
168 perature variation on the surface. Capillary fringes near the water/alkane table may be filled with  
169 water on Earth or alkane-rich liquid on Titan due to condensation of the atmosphere that pene-  
170 trates the vadose zone, but irrelevant in this work as they do not affect the stability of liquid col-  
171 umn as discussed later.

172 **3. Titan's surface liquids**

173 For evaluations purposes such as in this work, liquids on Titan's surface may be assumed  
174 to consist of three components (Tan & Kargel, 2018), while neglecting trace constituents, and be  
175 in vapor-liquid equilibrium (VLE) with the atmosphere with an overall composition of (Tan et  
176 al., 2013): 94.3462% nitrogen, 5.65% methane, and 0.0038% ethane. Using PC-SAFT, the com-  
177 position and density of surface liquids at 94 K and 1.467 bar for low-latitude regions, and 90 K  
178 and 1.467 bar for high-latitude regions, are listed in Table 1. The PC-SAFT parameters of all  
179 components are taken from Tan & Kargel (2018) along with the associated binary interaction  
180 parameters, except for that of nitrogen/ethane, which is set to 0.045 in this work to accommodate  
181 the mixture behavior at temperatures in subsurface that is much higher than that on Titan's sur-  
182 face. Consequently, entries in Table 1 may be slightly different from that in our previous works  
183 (Tan et al., 2013; 2015). For the record, Cordier et al. (2021) used a value of 0.07 for this binary

184 parameter, which is inaccurate in describing the liquid phase of nitrogen/methane/ethane ternary  
 185 mixtures in high temperature range of interest as shown in Appendix B.

186 As seen in Table 1, the composition of the liquids is ethane-rich in low latitudes and me-  
 187 thane-rich in high latitudes. Even though the temperature is lower in high latitudes, the liquid  
 188 density is also lower compared to that in low latitudes due to the more abundant methane (Tan et  
 189 al., 2015). These surface liquids may come from rainfalls and then flow down to subsurface  
 190 through large pores and fractures as recharge to the alkanofers. During the flow and after settling  
 191 down, they are subject to temperature gradient arising from geothermal activities of the moon.  
 192 Some of the liquids are inevitably trapped in smaller pores, which become smaller with depth  
 193 due to compaction. However, pores may migrate to warmer location (Smoluchowski &  
 194 McWilliam, 1984) in water ice, thus in the lower crust due to thermal gradient, so that small  
 195 pores may still be expected to exist in the deep.

196 **Table 1.** Properties of Titan's liquid on the surface in low- and high-latitude regions at atmos-  
 197 pheric pressure of 1.467 bar in VLE with the atmosphere

| Surface tem-<br>perature | Composition (mole%) |         |        | Density<br>[kg/m <sup>3</sup> ] |        |
|--------------------------|---------------------|---------|--------|---------------------------------|--------|
|                          | Nitrogen            | Methane | Ethane |                                 |        |
| Low latitudes            | 94 K                | 6.97    | 36.73  | 56.30                           | 596.08 |
| High latitudes           | 90 K                | 20.39   | 70.04  | 9.57                            | 544.82 |

198 Another possibility is that nitrogen and methane have an endogenic origin so that upward  
 199 migration from subsurface towards the surface may be expected until reaching a steady state. In  
 200 this work, the stability of columns in unconfined zone is evaluated at conditions after the steady  
 201 states are established regardless of either the liquid originates from recharge inflow from precipi-  
 202 tation on the surface or outflow of endogenic fluid from the deep. The liquid properties in the

203 column should be the same for both cases as the liquid also maintains equilibrium with the at-  
 204 mosphere on the surface.

205 **4. Modeling methods**

206 *4.1. Equilibrium in gravitational field with heat diffusion*

207 It has long been known that convection-free fluid columns in a single stable phase a sub-  
 208 ject to gravity  $g$  and a temperature gradient must have conditions according to an extended Gibbs  
 209 equation (Galliero et al., 2017). The change of chemical potential for each component  $i$  of the  
 210 fluid mixture along the column must be modified by the gravitational potential due to the change  
 211 of its depth ( $dh$ ) and its thermal diffusion due to the change of temperature ( $dT$ ):

$$212 \quad d\mu_i^\alpha = M_i g dh - \frac{Q_i}{T} dT, \quad i = 1 \dots N \quad (1)$$

213 where  $M_i$  is the molar mass of component  $i$ ,  $g$  is the gravity ( $= 1.352 \text{ m/s}^2$  for Titan),  $T$  is temper-  
 214 ature,  $Q_i$  is the heat due to the diffusion of component  $i$ , and  $N$  is the number of components ( $N =$   
 215 3 in this work).

216 For the thermal diffusion, instead of applying diffusion coefficients, the experimental da-  
 217 ta of which are scarce at low temperatures, the equation derived from the internal energy is in-  
 218 stead used for this work (Firoozabadi et al., 2000):

$$219 \quad \frac{Q_i}{RT} = -\frac{\bar{U}_i^R}{4RT} + \frac{1}{4RT} \frac{\bar{v}_i}{\sum_j z_j \bar{v}_j} \sum_j z_j \bar{U}_j^R, \quad i = 1 \dots N \quad (2)$$

220 where  $\bar{U}_i^R$  and  $\bar{v}_i$  are the partial molar residual internal energy and the partial molar volume of  
 221 component  $i$  in the mixture, respectively, which can be calculated using any suitable EOS (see  
 222 Appendix C). In Eq (2),  $\mathbf{z} = \{z_i, i = 1 \dots N\}$  is the composition and  $R$  is the gas constant. This ap-  
 223 proach was considered more accurate and efficient in a comparison study by Nikpoor et al.

224 (2013) than two other popular approaches, i.e., Haase's (1969) and Kemper's (1989) models.  
 225 Haase's approach was applied for Titan's subsurface liquids in a recent paper (Cordier et al.,  
 226 2021) while Firoozabadi's as in Eq (2) was also applied in our presentation (Tan & Kargel,  
 227 2020). For interested readers, the comparison between the performances of these two approaches  
 228 is shown in Appendix B. As mentioned earlier, both works used PC-SAFT as the main EOS,  
 229 which has been successfully applied for Titan's fluids (Tan et al., 2013; 2015; Luspay-Kuti et al.,  
 230 2015; Stevenson et al., 2015; Singh et al., 2017; etc.). The algorithm used for the thermo-  
 231 gravitational effects in this work is given in Appendix D.

232 *4.2. Capillary pressure*

233 Capillary pressure results from the strong adhesive interaction between the solid pore  
 234 wall and the fluid molecules confined inside the pore. Because of it, the fluid can be condensed  
 235 as a liquid-like phase and held strongly inside the pore. Only if there is a sufficient overpressure  
 236 axially across the pore that overcomes the capillary pressure, can the fluid be expelled and re-  
 237 leased from the pore. Without the overpressure, the entrapped fluid keeps any potential flows  
 238 from passing across the porous medium. On Earth, such trapping mechanism occurs with hydro-  
 239 carbon fluids due to capillary pressure of water confined in small pores of aquitards (England et  
 240 al., 1987). By analogy, Titan's subsurface liquids are trapped due to the capillary pressure of the  
 241 liquid in small pores forming an alkanotard.

242 The pores are commonly modeled as long thin open cylinders with radius  $r_p$ , in which the  
 243 capillary pressure by the wall on the fluid may be calculated using the Young-Laplace (YL)  
 244 equation:

$$245 P_{\text{cap}} = P^L - P^V = \frac{2\gamma^{\text{LV}}}{r_p} \cos \theta \quad (3)$$

246 where  $P^L$  is the pressure of the liquid-like phase inside the pores and  $P^V$  is the pressure of bulk  
 247 vapor thermodynamically in equilibrium with the liquid. Note that the calculations of capillary  
 248 pressure in this model require the assumption of the existence of vapor and liquid in equilibrium  
 249 but does not necessarily imply an actual phase equilibrium. In Eq (3), the fluid-wall interaction is  
 250 represented by the surface tension  $\gamma^{LV}$  that separates the liquid from the vapor, which can be cal-  
 251 culated using the simple parachor equation (Danesh, 1998):

$$252 \quad \gamma^{LV} = \left( \sum_i x_i \phi_i \rho^L - \sum_i y_i \phi_i \rho^V \right)^4 \quad (4)$$

253 where  $\rho^L$  and  $\rho^V$  are the densities of the coexisting phases, i.e., the liquid in the pores and the  
 254 bulk vapor, respectively.  $\phi_i$  is the parachor of component  $i$  tabulated in Appendix E, while  $x_i$   
 255 and  $y_i$  are the mole fractions of component  $i$  in the liquid and vapor, respectively.

256 In small pores of nanometer size, the extreme strength of the fluid-wall interaction is de-  
 257 scribed using a zero contact-angle  $\theta = 0$ , i.e., the pore wall becomes completely wet, and an ef-  
 258 fective pore radius  $r_e$  instead of the physical radius  $r_p$  (Tan & Piri, 2015):

$$259 \quad r_e = r_p (1 - \lambda(T, r_p)) \quad (5)$$

260 so that the capillary pressure in nanopores is calculated using the modified YL equation:

$$261 \quad P_{cap} = \frac{2\gamma^{LV}}{r_e} \quad (6)$$

262 The correction parameter  $\lambda$ , which depends on  $T$  and  $r_p$ , can be interpreted as the reduc-  
 263 tion of pore size due to adsorption layering that precedes the capillary condensation. Because of  
 264 the lack of experimental data of this layering,  $\lambda$  is commonly derived from experimental capil-  
 265 lary-condensation data. For this work, all  $\lambda$  parameters of the individual component of the mix-

ture are given in Appendix E for a typical porous media. For mixtures, the mixing rule for these  $\lambda$  parameters is the simple average  $\lambda = \sum(x_i \lambda_i)$ .

As usual, the vapor-liquid equilibrium for calculating capillary pressure in Eq (6) is carried out using the equality of chemical potentials but with different pressures of the equilibrium phases as expressed in Eq (3) or Eq (6). For further details, the readers are referred to Tan & Piri (2015), which applied PC-SAFT coupled with Eq (6), thus the name PC-SAFT/Laplace EOS. For fluid mixtures in vast amount of porous medium, such as that in subsurface crusts, the phase equilibrium for calculating the capillary pressure occurs at the bubble point as required by material balance (Tan et al., 2019a).

For the record, if the vapor and liquid in the equilibrium are assumed to be an ideal gas and incompressible liquid, respectively, Eq (3) reduces to a well-known approximation, i.e., the Kelvin equation, which was applied by Voss et al. (2007) to describe the capillary effects on Titan's methane liquid. However, both assumptions are inapplicable for Titan's fluids, so that the more general Eq (6) is to be used for more realistic calculations. The assumption of ideal gas has been proven inaccurate by the failure of modified Raoult's law (Tan et al., 2013), while the liquid is undoubtedly compressible as evident in its pressure-dependent densities (Tan et al., 2015).

## 5. Results and Discussion

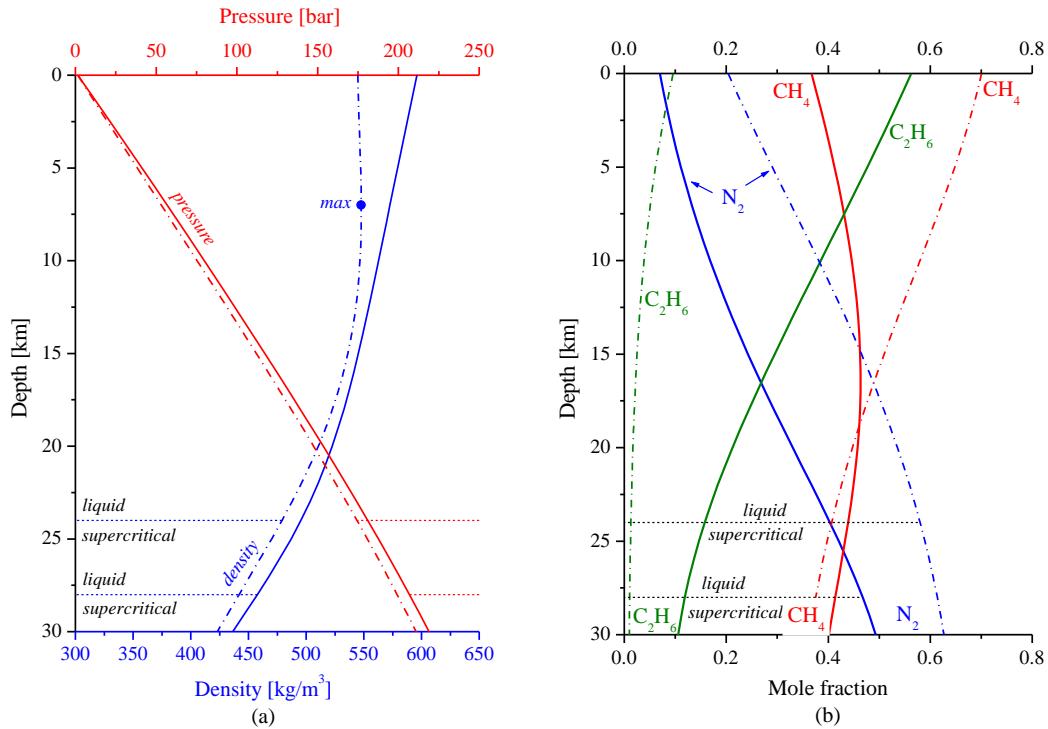
With a temperature profile and surface-liquid composition as inputs, the thermo-gravity algorithm described in section 4.1 straightforwardly provides the pressure gradient, density profile, and the corresponding composition grading with depth in unconfined alkanofers, which are in constant communication with the atmosphere above the liquid column.

### 5.1. Subsurface liquids in unconfined alkanofers

288 The calculations were first made for two temperature gradients available in the literature  
289 (Kalousova & Sotin, 2020) representing two different types of crust, i.e., water-ice crust and me-  
290 thane clathrate crust. For the latter, the case of 15-km thick clathrate crust is used, so that both  
291 crusts serve the calculations as the limiting cases for a range of properties resulting from clath-  
292 rate thickness up to 15 km on top of the water-ice shell. The temperature gradients are for low-  
293 latitude regions with a surface temperature of 94 K. Later, for high-latitude regions with a sur-  
294 face temperature of 90 K, the gradients are derived from the low-latitude cases as described in  
295 Appendix A. The calculated pressure gradient, density profile, and the composition grading of  
296 the subsurface liquid with those thermal gradients are presented in Figs. 2 and 4 for water-ice  
297 and methane-clathrate crusts, respectively; both also showing cases in low and high latitudes  
298 with properties of surface liquids as listed in Table 1.

299 As shown in Fig. 2(a), even though the pressure gradients in low and high latitudes are  
300 similar to each other, the density behavior is quite different. It decreases monotonically with  
301 depth in low latitudes while it increases with depth in the first few kilometers in high latitudes  
302 with a maximum at a depth of 7 km before decreasing. As mentioned earlier, such a reverse den-  
303 sity profile leads to convective instability as the lighter lower liquids would tend to migrate up-  
304 ward due to buoyancy. This situation is where crust with small pores in the deep can contribute  
305 to keep the liquid columns stable. The small pores in the crust can provide the trapped liquid suf-  
306 ficient capillary pressures to seal the space underneath thus blocking the upward convection, so  
307 that the crust layer factually acts as an alkanotard. In this case, any bulk liquid below the alka-  
308 notard stays in a confined alkanofe, the total pressure of which will increase by a portion or the  
309 whole weight of the crust above it, depending on the crustal structure. The analogy with Earth's

310 hydrocarbon reservoir is almost exact except that the liquid plugging the pores on Earth is usual-  
 311 ly water.



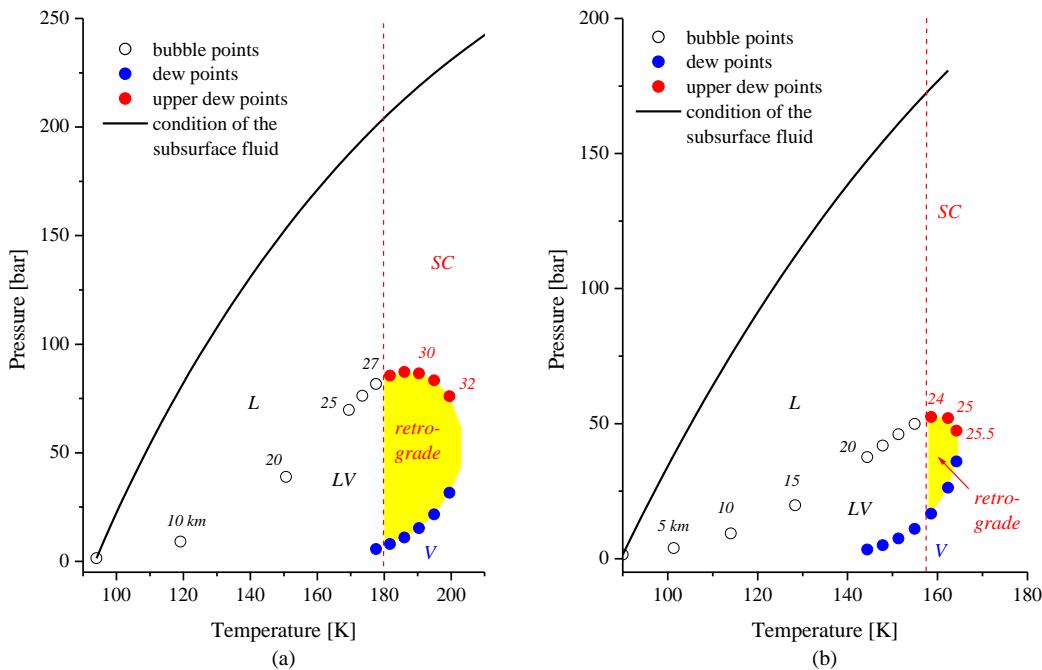
312  
 313 **Fig. 2.** Vertical profiles of subsurface liquid column in water-ice crust: (a) pressure and density;  
 314 (b) composition. The dash-dotted and solid curves are for high and low latitudes, respectively.  
 315 The liquid becomes supercritical at the depth of 28 km (low latitudes) and 24 km (high latitudes).

316 For the composition gradients shown in Fig. 2(b), regardless of the latitudes, the liquids  
 317 become nitrogen-rich and ethane-lean in the deep when they become supercritical despite their  
 318 pronounced differences on the surface. Because nitrogen is the most volatile component and  
 319 ethane is the least volatile component in the mixture, the thermal effect apparently dominates  
 320 over the gravitational one for Titan's liquids. The composition grading for high-latitude regions  
 321 in the first 10 km of depth may be compared with that from Cordier et al. (2021), where the pro-  
 322 files of nitrogen and ethane are similar in both works. However, for methane, it decreases with

323 depth as seen in in Fig. 2(b) while Cordier's is almost constant. For ethane-rich liquid in the low-  
324 latitude regions, not discussed in Cordier et al. (2021), methane even increases in the first 10 km.

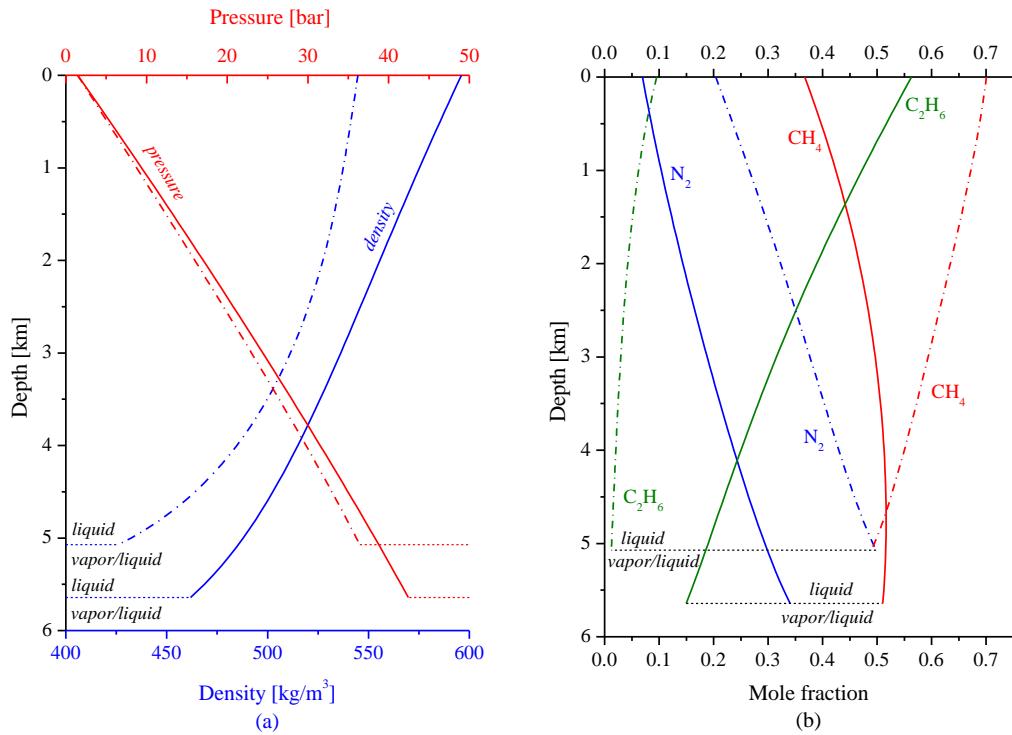
325 Another important feature shown in Fig. 2 is the occurrence of supercriticality at the  
326 depth of 28 km in low latitudes and 24 km in high latitudes. The pressure-temperature phase dia-  
327 gram corresponding to Fig. 2 is shown in Fig. 3. The supercritical region is at pressures and tem-  
328 peratures above the critical point of the mixture, i.e., the point where the upper dew-point curve  
329 meets the bubble-point curve. The shaded area surrounded by dew points is the so-called retro-  
330 grade region, a well-known phenomenon in oil/gas recovery where the mixture condenses upon  
331 depressurizing. In the figure, the dew- and bubble-point curves are calculated at the composition  
332 according to the grading with depth. When the liquid becomes supercritical, its properties change  
333 dramatically from the original liquid phase, particularly in its ability to effuse porous crust much  
334 easier, regardless of the existing pressure. In other words, the fluid can migrate vertically upward  
335 easier due to the buoyancy and can later accumulate in an upper space confined by alkanotards,  
336 thus resembling oil/gas reservoirs on Earth.

337 As the pressure builds up, a sufficient overpressure from below may exceed the capillary  
338 pressure so that upward leakage may occur across the alkanotard. This seal failure does happen  
339 on Earth with hydrocarbon seeps, where oil and natural gas escape the reservoir and flow slowly  
340 through network of cracks to the surface (Gluyas & Swarbrick, 2004). All these high-pressure  
341 mechanisms might facilitate the slow, continuous supply of methane to Titan's atmosphere, thus  
342 replenishing methane that is destroyed by photolysis. It offers a mechanism alternative to cry-  
343 ovolcanic eruptions (Lopes et al., 2013) as well as outgassing due to the decomposition of me-  
344 thane clathrate hydrates (Choukroun et al, 2010). The latter two mechanisms have long been  
345 thought to bring methane and other hydrocarbons from the interior to the surface.



346  
 347 **Fig. 3.** Supercritical region associated with Fig. 2 at: (a) low latitudes; (b) high latitudes. (L =  
 348 liquid; SC = supercritical; V = vapor; LV = liquid-vapor two-phase region).

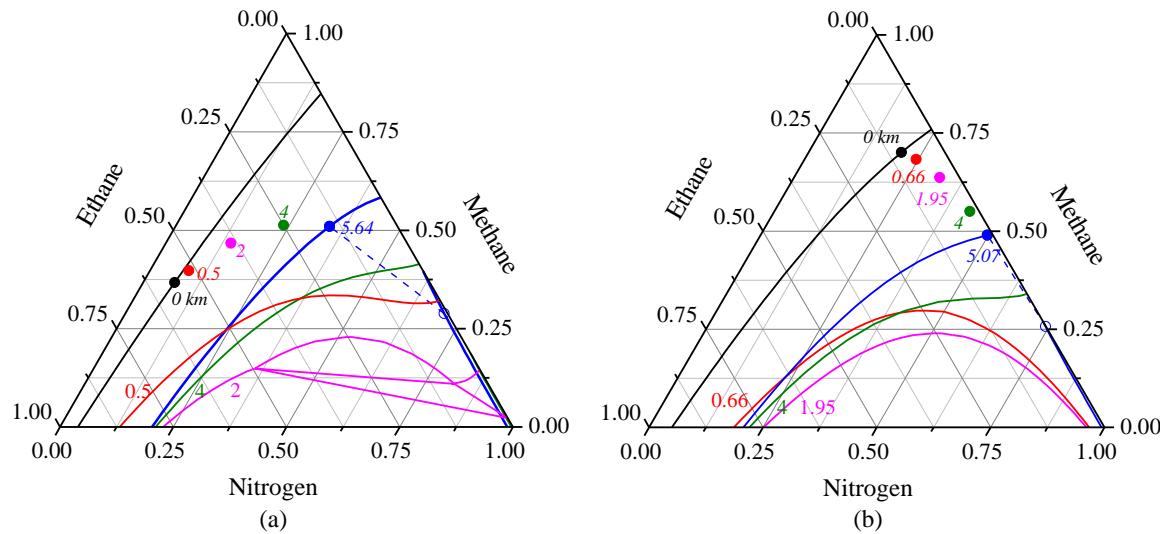
349 For methane-clathrate crusts, the vertical profiles of subsurface liquids are shown in Fig.  
 350 4. As the temperature gradient is larger, the liquid density monotonically decreases with depth in  
 351 all latitudes, and furthermore, if the mixture can stay in deeper location, it even splits into two  
 352 phases, liquid and vapor, at the depth of 5.64 km in low latitudes and 5.07 km in high latitudes.  
 353 Consequently, the existing liquid columns are shallower, and the composition grading ends with  
 354 methane-rich liquid prior to the phase split. Similar to the supercriticality in the previous case,  
 355 vapor is much more mobile than liquid to migrate upward thus introducing vertical instability to  
 356 the column. Again, capillaries with entrapped liquid can seal and block the flow, which may  
 357 eventually lead to accumulation with vapor on top of the liquid if empty space is available below  
 358 the seal, analogous to gas and oil reservoirs with cap rock on Earth. Another important behavior  
 359 is that even the ethane-rich surface liquid in the low latitudes quickly becomes ethane-lean not  
 360 far from the surface (~4 km).



361  
 362 **Fig. 4.** Vertical profiles of subsurface liquid column in methane-clathrate crust: (a) pressure and  
 363 density; (b) composition. The dash-dotted and solid curves are for high and low latitudes, respec-  
 364 tively. The liquid splits into two phases (in equilibrium with vapor) at the depth of 5.64 km at  
 365 low latitudes and 5.07 km at high latitudes.

366 Fig. 5 shows the ternary composition phase diagrams that correspond to the profiles in  
 367 Fig. 4. The progression of the composition at some depths is plotted as circles in the figure start-  
 368 ing from the surface (0 km). The associated phase boundaries at each depth are shown as curves,  
 369 most of which are bubble-point curves that move faster with depth towards nitrogen-rich region  
 370 than the composition grading do. This means that the composition is firmly in liquid region in  
 371 the first few kilometers. However, as the location goes deeper, the bubble-point curves reverse  
 372 the direction and meet the composition progression at the depth where the phase split into vapor  
 373 and liquid occurs. For the records, before the reversal, a second liquid appears on the diagram  
 374 introducing a liquid-liquid and even a three-phase vapor-liquid-liquid region at the methane-lean

375 side of the diagram. For clarity, the three-phase triangular region is only shown in panel (a) for  
 376 the depth of 2 km and the liquid-liquid regions without three-phase region are only shown in  
 377 panel (b) for the depths of 0.66 km and 1.95 km. Considering that the composition-grading paths  
 378 are never even close to liquid-liquid region, let alone the three-phase region, Titan's subsurface  
 379 liquid will never have a second liquid phase in equilibrium with it. Therefore, any subsurface  
 380 flow must be in a single phase, i.e., liquid or supercritical, or in two phases vapor and liquid.



381  
 382 **Fig. 5.** Composition phase diagrams as one descends into methane-clathrate crust from the sur-  
 383 face in: (a) low latitudes; (b) high latitudes. Curves: phase boundaries at various depths; points:  
 384 the corresponding liquid composition due to thermo-gravity effects. Vapor regions are very thin  
 385 with tiny amounts of ethane. Broken lines: tie lines connecting equilibrium compositions of liq-  
 386 uid and vapor. See the text for more details.

387 Table 2 shows the properties of subsurface liquids at points where bubble or supercriti-  
 388 cality is first encountered for all cases discussed above. Upon comparison with the surface condi-  
 389 tions in Table 1, the liquid at the phase boundaries is ethane-lean with mole fraction of ethane  
 390 less than 15 mole%, regardless of the conditions on the surface. Nitrogen is also the dominant

391 component in the liquid, except for the case of methane-clathrate crust in low latitudes, in which  
 392 methane is dominant. In all cases of water-ice and methane-clathrate crusts, methane is present in  
 393 substantial fractions in the deep.

394 **Table 2.** Properties of Titan's subsurface liquid in low and high latitudes at depths where the liq-  
 395 uid is about to bubble or become supercritical

| Latitudes                                    | Depth<br>[km] | <i>T</i> [K] | <i>P</i> [bar] | Composition (mole%)* |                  |                               | Density<br>[kg/m <sup>3</sup> ]* |
|--|---------------|--------------|----------------|----------------------|------------------|-------------------------------|----------------------------------|
|  |               |              |                | N <sub>2</sub>       | CH <sub>4</sub>  | C <sub>2</sub> H <sub>6</sub> |                                  |
| <i>Methane-clathrate crust: bubble point</i> |               |              |                |                      |                  |                               |                                  |
| Low  | 5.64          | 155.2        | 42.44          | 34.02<br>(70.43)     | 51.00<br>(28.82) | 14.98<br>(0.75)               | 461.8<br>(138.7)                 |
| High   | 5.07          | 145.0        | 36.43          | 49.82<br>(74.23)     | 48.96<br>(25.70) | 1.22<br>(0.07)                | 425.9<br>(134.9)                 |
| <i>Water-ice crust: supercritical</i>        |               |              |                |                      |                  |                               |                                  |
| Low  | 28.0          | 181.8        | 206.8          | 46.76                | 41.37            | 11.87                         | 457.7                            |
| High   | 24.0          | 158.6        | 174.3          | 58.02                | 40.68            | 1.30                          | 479.1                            |

396 \* The values in parentheses are the properties of vapor in equilibrium with liquid when the first bubbles appear.

397 For water-ice crust in high latitudes, the density increases with depth in the first 7 km as  
 398 illustrated in Fig. 2, but then decreases afterwards so that liquids below the depth of 7 km are  
 399 subject to convection. In fact, there is a maximum temperature gradient that provides monoton-  
 400 ically increasing density profile at least until the water-ice crust reaches the bottom of the stag-  
 401 nant lid, below which the crust is no longer conductive. The maximum temperature gradient can  
 402 be shown using the method in Appendix A to be introduced by a conductive water-ice crust that  
 403 has a heat flux of  $q_0 = 3.90 \text{ mW/m}^2$  for low-latitude case, and  $6.05 \text{ mW/m}^2$  for high-latitude case,

404 to maintain the stability of liquid columns at least until the bottom of stagnant lid without the as-  
405 sistance of capillary pressure. The values of  $q_0$ , however, are much lower than that to produce the  
406 42-km thick stagnant lid, i.e.,  $13.1 \text{ mW/m}^2$  (Kalousova & Sotin, 2020), and for the low-latitude  
407 case it is even less than that due to radiogenic heating, which is  $4.35 \text{ mW/m}^2$  on the surface (For-  
408 tes, 2012). This contradiction implies that temperature gradients resulting from these values of  $q_0$   
409 cannot be realistic, thus further emphasizing the crucial role of capillary pressures in helping to  
410 create the column stability in the subsurface with heat flux much larger than  $q_0$ .

411 *5.2. Capillary pressure*

412 As discussed earlier, capillary pressure of liquids confined in small pores may help to  
413 maintain the stability of the liquid column if a vertical instability is happening. While pores with  
414 radii of  $1 - 25 \text{ nm}$  can be present in water ice at low temperatures (Raut et al., 2007), pore sizes  
415 decrease with depth due to compaction but with an unknown profile. Therefore, a small pore size  
416 may be applied to represent pore sizes in large depths as a limiting case. A physical pore radius  
417 of  $2.2 \text{ nm}$  is chosen for calculations in this work due to the availability of reliable experimental  
418 data required for the derivation of parameter  $\lambda$  in Eq (5), which are given in Appendix E. For flu-  
419 id mixtures, as previously pointed out, the capillary pressure is calculated at their bubble points,  
420 thus at the same composition as the liquid outside the pores.

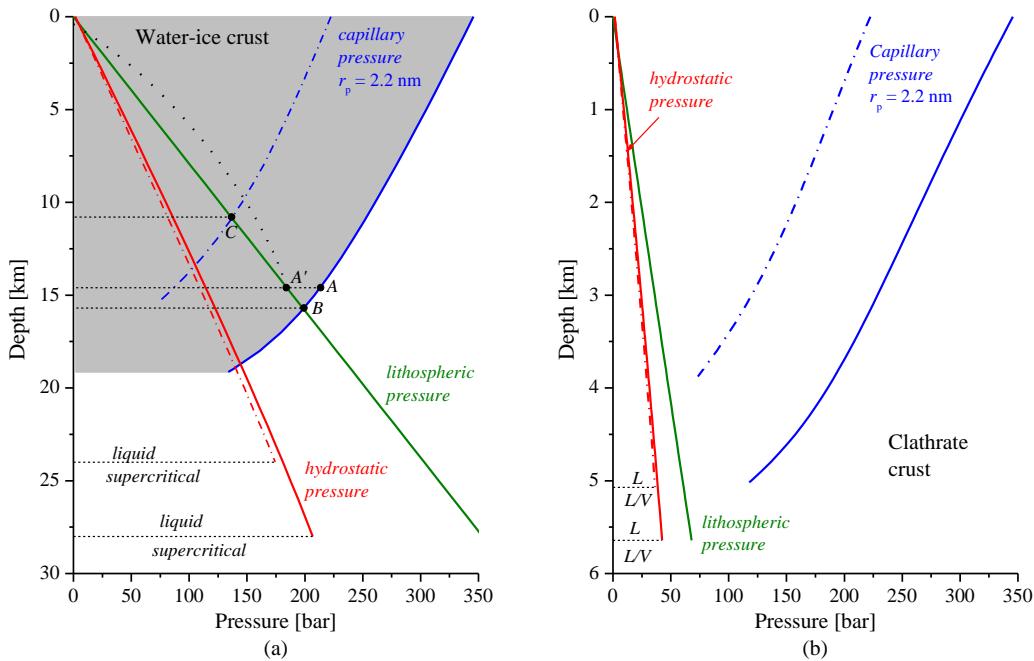
421 In fact, porous mediums statistically exist with pore-size distributions (PSD) from small  
422 to large sizes, with the largest ones most susceptible to leakage due to the lowest capillary pres-  
423 sure they can impose on the entrapped liquids. Therefore, for leakage analysis, only the largest  
424 pores in the PSD matter. Fig. 6 shows the capillary pressures of liquids trapped inside pores of  
425 possible alkanotard with constant radii of  $2.2 \text{ nm}$ , which may be considered here as the largest  
426 pores in the PSD at any depths for the analysis. If the largest pores in the PSD have radii much

427 larger than 2.2 nm and the pore size decreases with depth due to compaction, the capillary pres-  
428 sure is roughly like the dotted curve plotted in Fig. 6 in comparison with the solid curve for the  
429 low-latitude case. As pore size decreases with depth, the capillary pressure is lower near the sur-  
430 face and higher in the deep. This dotted curve is for illustration only, not calculated due to the  
431 unknown dependency of pore size on pressure/depth. Since the capillary pressure even vanishes  
432 in very large pores, where the liquid behaves like in the free bulk, as long as the stability is con-  
433 cerned, liquids confined in larger pores near the surface, such as that in capillary fringes at the  
434 bottom of vadose zone, is irrelevant. Even if smaller pores exist in the region, many larger pores  
435 or even large fractures are available, thus still allowing migration from underneath to the surface.

436 The hydrostatic pressure of the liquid column and the lithospheric pressure due to the  
437 weight of the crust are also shown in Fig. 6 for comparison. The latter is the maximum value by  
438 assuming nonporous crust with a constant density of  $934 \text{ kg/m}^3$  for water ice (at 93 K – Lide,  
439 2005) and  $890 \text{ kg/m}^3$  for methane clathrate (below 273 K – Makogon, 2010). In fact, the crusts  
440 are porous, so their actual density must be lower, regardless of the ability of their pores to store  
441 some liquids, which are lighter than the crusts, i.e., less than  $600 \text{ kg/m}^3$  as shown by the liquid  
442 density in Figs. 2(a) and 4(a). Note that all calculations here are for evaluation purposes, thus  
443 providing only rough values to illustrate the order of magnitude of various pressures that can ex-  
444 ist in subsurface liquid column. Therefore, it is justifiable here to use the maximum possible lith-  
445 ospheric pressure due to the unknown porosity of the crust.

446 When liquid is trapped in a confined alkanofluid under an alkanotard by capillary pressure,  
447 its pressure increases by full lithospheric pressure or just a portion of it. The latter occurs when  
448 the crust structure can support some weight of the overlying burden. Without the support, the  
449 liquid is “squeezed” by the full burden. This lithospheric pressure can introduce an overpressure

450 from below the alkanotard, but no upward leaks can occur as long as the capillary pressure that  
451 seals the alkanotard is higher. Such leaks may potentially occur if the opposing pressures are al-  
452 most equal in magnitude with slight overpressure. In the situation shown in Fig. 6(a), for exam-  
453 ple, if an alkanotard of water-ice crust with a largest pore size of 2.2 nm exists at a depth of 14  
454 km in low latitudes (point A), no upward leaks can occur because the lithospheric pressure at this  
455 depth (point A') is smaller than the capillary pressure at point A. However, if such an alkanotard  
456 exists at a depth of 16 km (point B), upward leaks would occur as the capillary pressure may  
457 now be overcome by slight overpressure due to the lithosphere. Thus, the depth of alkanotard  
458 that allows such leaks can be as shallow as 11 km (point C) in high latitudes, but deeper at 16 km  
459 in low latitudes (point B). In other words, leakage is more likely to occur in high latitudes than  
460 low latitudes as the capillary pressure to overcome is lower at the same depth. However, if the  
461 largest pore size at a specified depth is larger than 2.2 nm, the capillary pressure is lower and can  
462 have values anywhere in the shaded area in Fig. 6(a) in low latitudes. For illustration, as men-  
463 tioned earlier, it may have a profile such as that shown by the dotted curve in Fig. 6(a), where the  
464 depth of the leaks is even shallower at point A' instead of point B. At these locations, a small  
465 overpressure from underneath would induce upward leaks. This small overpressure may result  
466 from a gradual implosion of the crust structure or additional geothermal activities from the deep  
467 that may lead to fluid volume expansion. Once the leaks occur, the escaping fluid becomes liquid  
468 phase as the rest of the bulk fluid outside the pores, then subject to the hydrostatic overpressure  
469 and the buoyancy due to density difference to flow upward, which are also the major mecha-  
470 nisms of upward migration for oil on Earth. Note that in this case, the liquid has not reached the  
471 supercriticality (at depths  $> 24$  km) when the leaks through 2.2-nm pores are allowed to happen  
472 at point B or C.



473  
474 **Fig. 6.** Capillary pressures of subsurface liquid columns if trapped inside small pores with con-  
475 stant  $r_p = 2.2 \text{ nm}$  in: (a) water-ice crust; (b) methane-clathrate crust. The dash-dotted and solid  
476 curves are for high and low latitudes, respectively. Profiles of capillary pressure end when the  
477 confined liquid reaches pore critical point in the deep. Read the text for the shaded area and dot-  
478 ted curve in panel (a). Profiles of hydrostatic and lithospheric pressures are also added to the plot  
479 for comparison.

480 In Fig. 6, the profiles of capillary pressure end at the respective pore critical point (Tan et  
481 al., 2019b; 2020), where the confined liquid become supercritical, thus introducing a dramatic  
482 drop of capillary pressure if not none, which effectively removing the trapping mechanism by the  
483 pores. This means, even though the capillary pressures are always higher above the depths of  
484 pore critical points in Fig. 6(b), upward migration can still occur at or below the critical-point  
485 depths due to the supercriticality in the confinement. Once the leaks occur, the escaping fluid  
486 also becomes liquid phase as the rest of the bulk fluid outside the pores and has the same fate as  
487 that in the water-ice crust. Note that in this case, the liquid has not reached the depth where the

488 phase split occurs (at depths > 5 km) when the leaks through 2.2-nm pores are allowed due to the  
489 supercriticality of the liquids confined in the pores.

490 **6. Conclusions and Remarks**

491 An algorithm for thermo-gravitational effects based on an extended Gibbs equation is ap-  
492 plied for calculations on the convection-free pressure/density gradients and composition grading  
493 of Titan's unconfined alkanofers in low and high latitudes, for porous water-ice and methane-  
494 clathrate crusts. Based on the resulting vertical profiles in both low and high latitudes, upon ap-  
495 plying temperature gradients proposed in the literature, the liquid density has reverse profiles  
496 where the density decreases with depth, which can introduce vertical convection due to buoyan-  
497 cy, thus instability of the liquid columns. In this case, the stability can be maintained if there are  
498 liquids trapped in small pores forming an alkanotard that seals the alkanofer from the top.

499 Regardless of the conditions of liquid on the surface in different latitudes, the composi-  
500 tion of subsurface liquid tends to be nitrogen-rich and ethane-lean in the deep. This behavior in-  
501 dicates that for a liquid column on Titan, the thermal effects dominate over the gravitational  
502 counterpart as nitrogen is the most volatile component while ethane is the least volatile, which  
503 prefer warmer/deeper and colder/shallower locations, respectively. On the other hand, methane is  
504 present in substantial amount in all depths. In the first 10-km depth for water-ice crust at high  
505 latitudes, the resulting composition grading is similar to that by Cordier et al. (2021), who ap-  
506 plied a different thermo-diffusion model, except for decreasing methane instead of being almost  
507 constant.

508 For Titan's subsurface liquids in water-ice and methane-clathrate crusts, the capillary  
509 pressure in alkanotard of the same depth that helps the stability is higher in low latitudes than in  
510 high latitudes so that upward leakage is more likely to occur in high latitudes at shallower loca-

511      tions. In any cases of this study, the subsurface liquids can leak upwards before they become su-  
512      percritical or split into vapor and liquid at deeper locations. When leakage happens, the liquid  
513      escapes from the reservoir to the surface, such as that with natural oil seeps on Earth, where oil  
514      and natural gas flow slowly through network of cracks to the surface (Gluyas & Swarbrick,  
515      2004). These seeps can be a potential mechanism that spreads widely on the surface and occurs  
516      very slowly, which facilitate the need for continuous or episodic supply of methane to Titan's  
517      atmosphere to prevent depletion due to photolytic reactions, as an alternative to cryovolcanism  
518      (Lopes et al., 2013) and outgassing from dissociation of clathrate hydrates (Choukroun et al.,  
519      2010), which have long been thought to bring methane and other hydrocarbons from the interior  
520      to the surface. The seeps may also be the source of the extensive wetlands suggested by Neish &  
521      Lorenz (2014) in their scenario on the elevation distribution of Titan's craters. Moreover, as  
522      found on Earth, hydrocarbon seeps support diverse biological activities (Joye, 2020), thus rele-  
523      vant to research of finding extraterrestrial life.

524      **Author statement**

525      ST: Conceptualization, Methodology, Software, Validation, Formal Analysis, Writing-Original  
526      Draft, Writing-Review & Editing.

527      HA: Conceptualization, Formal Analysis, Writing-Review & Editing.

528      **Declaration of competing interest**

529              The authors declare that they have no known competing financial interests or personal re-  
530      lationships that could have appeared to influence the work reported in this paper.

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 535 in the early stage of the work.

536 **Appendix A. Temperature gradient of conductive crusts**

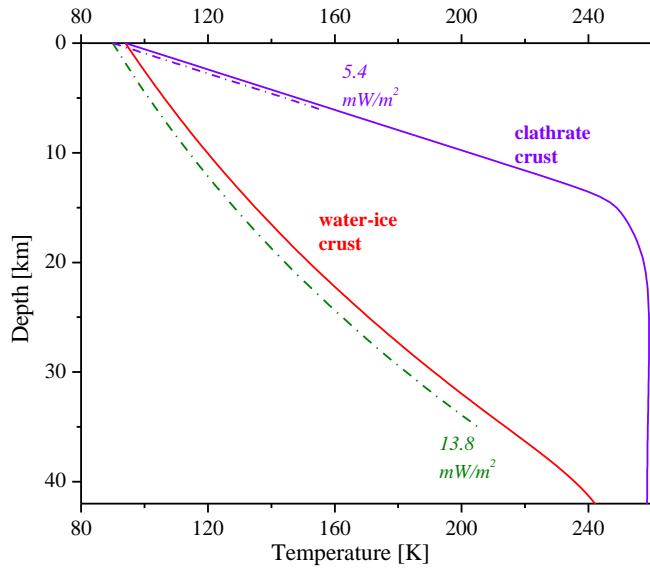
537 The temperature of subsurface liquids changes according to the temperature profile due to  
 538 conductive heat flux  $q$  within the crusts. The crust is assumed to be conductive in transferring  
 539 heat along the temperature gradient. Therefore, it depends on the properties of the crust material  
 540 as well as the heat flux  $q$  available from the deep.

541 
$$\frac{dT}{dh} = -\frac{q}{\kappa(T)} \quad (\text{A1})$$

542 where  $\kappa$  is the thermal conductivity of the crust. For methane-clathrate crust, the thermal conduc-  
 543 tivity is assumed to be constant at 0.5 W/m/K (Kalousova & Sotin, 2020). Using the constant  $\kappa$ ,  
 544 the gradient in 15-km thick methane-clathrate crust in Kalousova & Sotin (2020) can be calculat-  
 545 ed with a heat flux of 5.4 mW/m<sup>2</sup>. However, for water-ice crust (ice Ih), the conductivity varies  
 546 with temperature as (based on Ross & Kargel, 1998):

547 
$$\log \kappa(T) = 2.7154 - 0.9752 \log T \quad [\text{W/m/K}] \quad (\text{A2})$$

548 The assumption of thermal conductive equilibrium heat flux may be valid in shallow  
 549 crustal depths (upper tens of kilometers), where no solid-state convection is present. This as-  
 550 sumption is also valid for literature temperature gradients used in this work (Kalousova & Sotin,  
 551 2020) where the solid convection does not happen in the stagnant lid, i.e., until the temperature  
 552 exceeds 250 K, which is never reached in this work. The bottom of the stagnant lid is 42 km for  
 553 water-ice crust and 18.5 km for the 15-km thick clathrate crust (Kalousova & Sotin, 2020).



554

555 **Fig. A1.** Subsurface temperature gradients of Titan's crusts in low (solid curves) and high lati-  
 556 tudes (dash-dotted curves) applied in this work down to 42 km deep; the gradients in low lati-  
 557 tudes are directly taken from Kalousova & Sotin (2020).

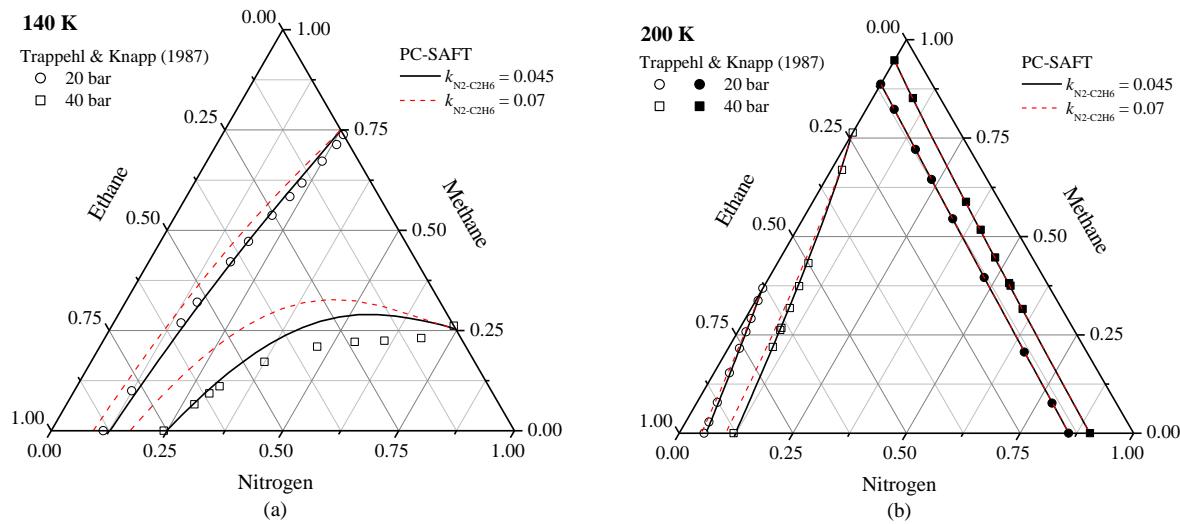
558 Fig. A1 presents all temperature gradients used in this work. Based on Eqs. (A1) and  
 559 (A2), the temperature gradients in water-ice crust can be calculated. For the gradients in Ka-  
 560 lousova & Sotin (2020), the heat is found to be  $13.8 \text{ mW/m}^2$ , while their heat is slightly smaller  
 561 at  $13.1 \text{ mW/m}^2$ , which may be due to different values of heat conductivity was used instead of  
 562 Eq (A2). However, this difference is not crucial for evaluation purposes in this work. While the  
 563 temperature gradients in low latitudes in Fig. A1(a) are directly taken from Kalousova & Sotin  
 564 (2020), the corresponding gradients in high latitudes are calculated using Eqs (A1) and (A2) with  
 565  $q = 13.8 \text{ mW/m}^2$  for water-ice crust, and  $5.4 \text{ mW/m}^2$  for methane-clathrate crust.

566 **Appendix B. Effects of using different binary parameters and thermo-diffusion approaches**

567 Fig. A2 shows the performance of PC-SAFT using the binary parameter for  $\text{N}_2/\text{C}_2\text{H}_6$  in  
 568 this work (0.045), compared to 0.07 that was used by Cordier et al. (2021), to describe the ter-

569 nary  $\text{N}_2/\text{CH}_4/\text{C}_2\text{H}_6$  in higher temperature range. As seen in the figures, the smaller binary parameter represents the experimental data (Trappehl & Knapp, 1987) better, particularly obvious in  
 570 the liquid phase.

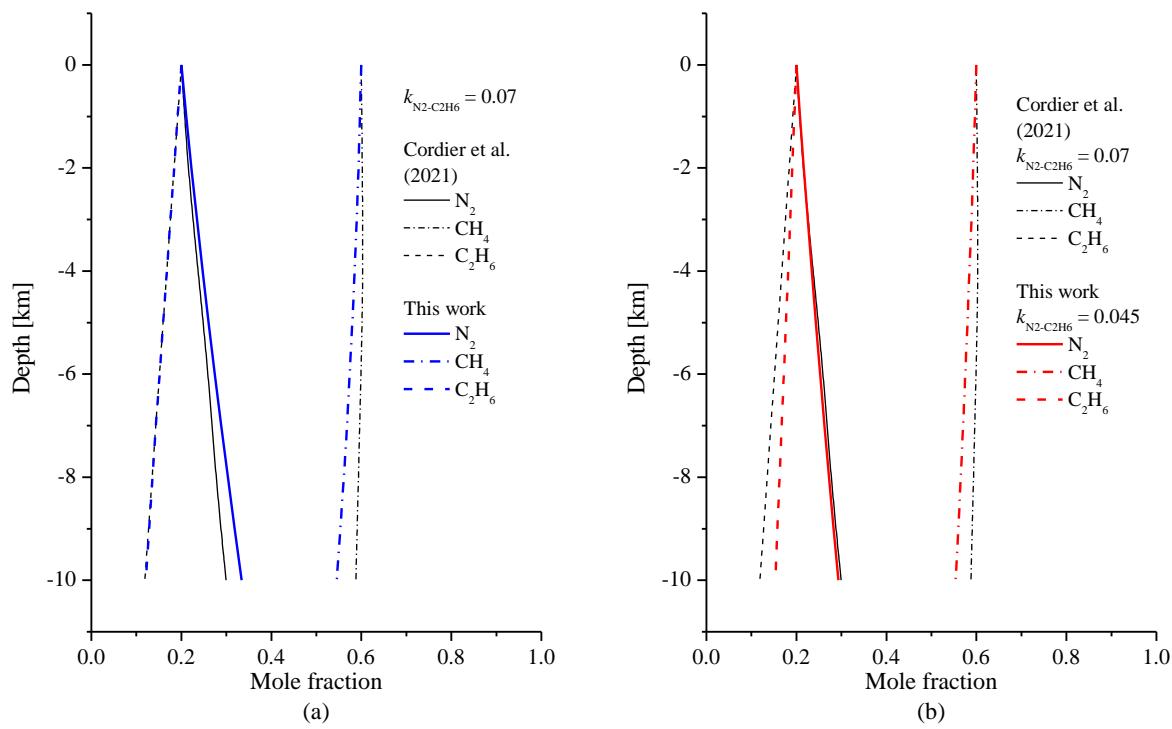
572 The thermo-diffusion approach used in Cordier et al. (2021) is also different from ours as  
 573 discussed in the paper. Since their surface composition is different from ours, we take the com-  
 574 position of case (b) in Figure 4 of their paper, which is the closest to our case for high-latitude  
 575 regions, for comparison here. All conditions are first also made the same, including the binary  
 576 parameter of  $\text{N}_2/\text{C}_2\text{H}_6$  above (0.07), but different approaches of the thermal diffusion. The results  
 577 are shown in Fig. A3(a), which reveal similar compositional grading within 10 km of depth.  
 578 While the gradient of  $\text{C}_2\text{H}_6$  is virtually the same, that of  $\text{N}_2$  and  $\text{CH}_4$  increase and decrease at  
 579 larger rates using the current approach, respectively. This discrepancy seems to get larger if the  
 580 subsurface location is deeper as it is in this work. As discussed in an evaluation by Nikpoor et al.  
 581 (2013), Firoozabadi's approach that we use is better than Haase's that Cordier et al. used.



582

583 **Fig. A2.** Performance of PC-SAFT for  $\text{N}_2/\text{CH}_4/\text{C}_2\text{H}_6$  using different binary parameter of  $\text{N}_2/$   
 584  $\text{C}_2\text{H}_6$ , 0.045 (this work) and 0.07 (Cordier et al., 2021) at: (a) 140 K; (b) 200 K. All other param-  
 585 eters are the same for the comparison. Liquid is near the ethane side while vapor is near the me-  
 586 thane side.

587 To see the discrepancy coming from using both different thermo-diffusion approach and  
 588 different binary parameter of  $\text{N}_2/\text{C}_2\text{H}_6$ , the calculation was repeated, and the results are shown in  
 589 Fig. A3(b). Obviously,  $\text{N}_2$  and  $\text{C}_2\text{H}_6$  are the components affected by the different parameters.  
 590 While  $\text{N}_2$  is now virtually the same,  $\text{C}_2\text{H}_6$  decreases at a lower rate for Firoozabadi's thermo-  
 591 diffusion approach.



592  
 593 **Fig. A3.** (a) Comparison of the results from different thermo-diffusion approach in this work  
 594 with that in Cordier et al. (2021). The conditions and all parameters are the same for the compar-

595 ison. (b) Comparison of the results if the binary parameter of N<sub>2</sub>/C<sub>2</sub>H<sub>6</sub> used in the calculations is  
 596 also different (0.045 versus 0.07).

597 **Appendix C. Partial molar properties**

598 There are two partial molar properties needed for diffusion-heat calculation in Eq (2), i.e.,  
 599 the partial molar residual internal energy and the partial molar volume of component *i* in the  
 600 mixture, respectively. They can be calculated by any EOS from the fugacity coefficient of com-  
 601 ponent *i* in the mixture ( $\hat{\phi}_i$ ) through the following expressions.

602 Partial molar internal energy of component *i*:

$$603 \quad \bar{U}_i^R = -T \left( \frac{\partial \ln \hat{\phi}_i}{\partial T} \right)_{\rho, \mathbf{z}} - P \left( \frac{\partial \ln \hat{\phi}_i}{\partial P} \right)_{T, \mathbf{z}} \quad (A3)$$

604 Partial molar volume of component *i*:

$$605 \quad \frac{\bar{v}_i}{RT} = \left( \frac{\partial \ln \hat{\phi}_i}{\partial P} \right)_{T, \mathbf{z}} + \frac{1}{P} \quad (A4)$$

606 **Appendix D. Algorithm for thermo-gravitational effects**

607 For numerical calculation purposes of pressure gradient and compositional grading, it is  
 608 useful to slice the liquid into imaginary layers: 1, 2 ... *k*-1, *k*, as illustrated in Fig. A4. In this  
 609 case, Eq. (1) may be formulated for individual layers in terms of fugacity calculated at the aver-  
 610 age temperature  $T(h_{k,k-1})$  estimated at the middle point within the layer  $h_{k,k-1} = \frac{1}{2}(h_k + h_{k-1})$ . The  
 611 fugacity of component *i* at *k*-th layer at a depth of  $h_k < 0$  can be calculated from the previous (*k*-  
 612 1)-th layer that is closer to the surface (Galliero et al., 2017):

$$613 \quad \hat{f}_{i,k}^{\alpha}(T(h_k), \mathbf{z}_k, P_k) = \hat{f}_{i,k-1}^{\alpha}(T(h_{k-1}), \mathbf{z}_{k-1}, P_{k-1}) \exp \left( \frac{M_i g \Delta h_{k,k-1}}{RT(h_{k,k-1})} - \frac{Q_i}{RT(h_{k,k-1})} \frac{\Delta T_{k,k-1}}{T(h_{k,k-1})} \right) \quad (A5)$$

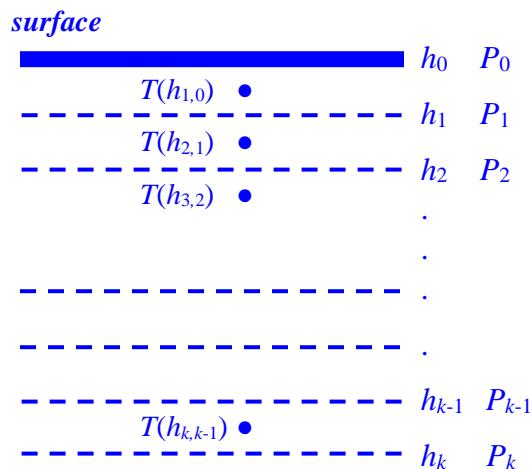
614 The computational layer thickness, is the difference between two consecutive depths:

615  $\Delta h_{k,k-1} = |h_k - h_{k-1}|$  (A6)

616 The temperature difference across each layer provided by the temperature profile of the crust is:

617  $\Delta T_{k,k-1} = T(h_k) - T(h_{k-1})$  (A7)

618 Eq (A3) is solved iteratively from the initial depth at  $h_0$ , down to a depth of  $h < h_0$ . The  
 619 initial depth  $h_0$  is the surface ( $h = 0$ ) at atmospheric pressure ( $P_0 = P_{\text{atm}}$ ). At a depth  $h$ , the tem-  
 620 perature is  $T(h)$  given by the temperature profile. The outputs of this calculation are the composi-  
 621 tional grading and pressure gradient due to the thermo-gravitational effects, and consequently the  
 622 corresponding liquid density.



623 **Fig. A4.** Intervals of depth, which may be considered as imaginary layers in liquid body for cal-  
 624 culations. Note that the average temperature in each layer is taken at the middle of the layer.

625 The problem in Eq. (A5) has  $N$  equations with  $N$  unknowns, i.e., the composition  $\mathbf{z}_k$  and  
 626 the pressure  $P_k$  for any  $k$ -th layer, as also recently pointed out by Baghooee et al (2021). The  
 627 mole fraction of the last component  $z_N$  can be obtained from the fact that  $\sum z_i = 1$  at any layers.  
 628 Therefore, this situation is analogous to that for phase-boundary calculations in VLE, i.e., dew  
 629 point or bubble point. The difference is that Eq (A5) has the exponential as well as different  
 630 pressures for the fugacities in the *same phase*. However, this difference does not prevent the

631 analogy to be manipulated so that the common phase-boundary algorithm can be readily applied  
 632 as described below.

633 As commonly done in phase-boundary calculations,  $K$ -values are defined as the ratios of  
 634 the equilibrium compositions, which are readily adopted for the current extension with thermo-  
 635 gravitational effect. Because the fluid is in a single phase, i.e., liquid, the compositions for an  
 636 imaginary layer are the total compositions of the upper ( $\mathbf{z}_u$ ) and the lower ( $\mathbf{z}_l$ ) boundaries of the  
 637 layer. The  $K$ -value of component  $i$  are expressed in terms of the fugacity coefficients:

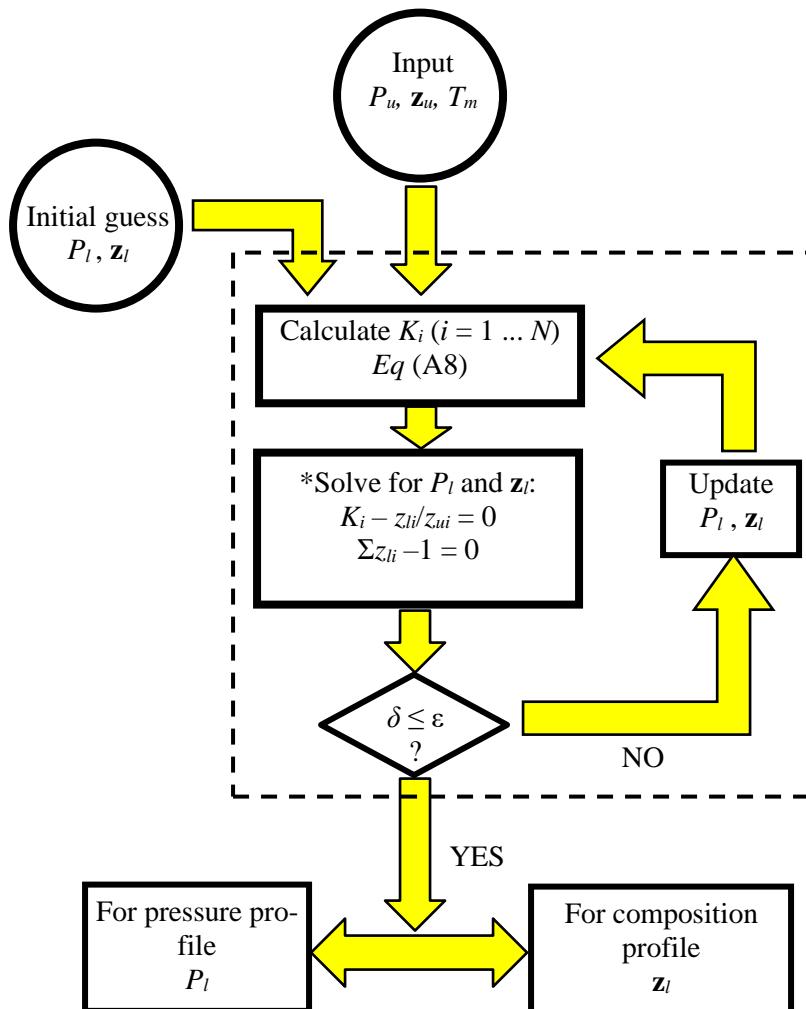
$$638 \quad K_i = \frac{z_{l,i}}{z_{u,i}} = \frac{\hat{\phi}_i^\alpha(T(h_{l,u}), z_u, P_u)}{\hat{\phi}_i^\alpha(T(h_{l,u}), z_l, P_l)} \frac{P_u}{P_l} \exp\left(\frac{M_i g \Delta h_{l,u}}{RT(h_{l,u})} - \frac{Q_i}{RT(h_{l,u})} \frac{\Delta T_{l,u}}{T(h_{l,u})}\right) \quad (\text{A8})$$

639 In solving Eq (A8) with known properties at  $h_u$ , the convergence at  $h_l$  is reached when all  
 640  $K$ -values are equal to unity as their analogous counterparts are in phase-boundary calculations.  
 641 The flow chart in Fig. A5 describes the computation as a root-finding of functions  $K_i - z_{l,i}/z_{u,i} = 0$   
 642 for all  $i$  subject to  $\sum z_{l,i} - 1 = 0$ , which is the routine of calculating dew/bubble points (inside the  
 643 dashed-line box). Solution using this approach needs only slight changes from the commonly  
 644 available coding for phase-boundary calculations: instead of using just the ratio of fugacity coef-  
 645 ficients as  $K_i$ , the ratio of different pressures and the exponential that contains the thermo-  
 646 gravitational effect must be added, as given in Eq (A8). Moreover, the properties involved in Eq  
 647 (A8) need their equivalence to be defined for the algorithm as follows.

648 The pressure at the lower layer  $P_l$  is the “phase-boundary” pressure to be calculated to-  
 649 gether with the corresponding composition  $\mathbf{z}_l = \{z_{l,i}\}$  analogous to the composition of the “incipi-  
 650 ent phase”. The terms in the quotation marks are well defined in the analogous phase-boundary  
 651 calculation. The lower layer in Eq. (A8) may be arbitrarily labeled as “liquid”, so that the “phase  
 652 boundary” in the calculation is the “dew point” and the “incipient phase” is “liquid phase”. Of

653 course, the reverse is also equally effective, i.e., if the lower layer is instead labeled as “vapor  
 654 phase”, then the “phase boundary” in the calculation is the “bubble point”, so that the “incipient  
 655 phase” is “vapor phase”.

656 It is worth noting that this algorithm does not specifically depend on the choice of EOS in  
 657 calculating the fugacity coefficients, nor the fluid mixtures and the planetary bodies. Therefore,  
 658 they can be considered as independent subroutines that are applicable for describing other fluids  
 659 on other planetary bodies, even if another accurate EOS is used.



660

661 **Fig. A5.** Flow chart for solving Eq. (A5) using a routine for iterative phase-boundary calculation  
 662 (inside the dashed-line box). \*Newton-Raphson method is used to calculate new values of  $P_l$  and

663  $\mathbf{z}_l$ , where  $\delta$  and  $\varepsilon$  are the error of the calculation method and a small number, respectively, as the  
 664 stopping criterion. Initial guesses of a higher pressure than  $P_u$  may be used, while that of compo-  
 665 sition may be made equal to  $\mathbf{z}_u$ .

666 **Appendix E. Parameters needed for capillary-pressure calculations**

667 The first group of parameters is the parachors for the surface-tension calculations in Eq  
 668 (4), which can all be derived from literature data of surface tension. The parachors are listed in  
 669 Table 3. Using these parachors, the calculated surface tension has the unit of mN/m (or dyne/cm)  
 670 if the densities are in mol/cm<sup>3</sup>.

671 **Table 3.** Parameters needed for capillary-pressure calculations

| Component $i$ | $\phi_i$ | $T_{Ci}$ [K] | $A_i$    |
|---------------|----------|--------------|----------|
| Nitrogen      | 60.50    | 126.192      | -1.19024 |
| Methane       | 71.95    | 190.564      | -1.93301 |
| Ethane        | 111.0    | 305.330      | -1.14895 |

672 The second group is the  $\lambda$  parameters of the individual component of the mixture needed  
 673 for the effective pore radius in Eq (5). Even though these parameters also depend on the material  
 674 type of the porous medium, for evaluation purposes in this work that only needs the order of  
 675 magnitude of the capillary pressure, silica MCM-41 that has effectively uniform pore size is used  
 676 in this work. MCM-41 is also commonly used in adsorption experiments for investigating con-  
 677 finement effects in engineering disciplines. Furthermore, a pore radius of 2.2 nm is chosen in this  
 678 work due to the reliability of capillary-condensation data for nitrogen in the literature that can be  
 679 used as benchmark for deriving the parameters of methane and ethane. The derivation procedure  
 680 is given in the Supplementary Material, while the resulting parameter for component  $i$  is in the  
 681 exponential form:

682 
$$\lambda_i(T) = \exp A_i \left( 1 - \frac{T}{T_{Ci}} \right) \quad (A9)$$

683 where  $T_{Ci}$  is the critical temperature of component  $i$ , and  $A_i$  is the coefficient derived from the  
684 experimental capillary-condensation data. Both  $T_{Ci}$  and  $A_i$  are given in Table 3.

685 **Appendix F. Supplementary Materials**

686 The supplementary file is available online. It contains the numerical values plotted in the  
687 figures, the derivation procedure of parameter  $\lambda$ , and the codes of thermo-gravitational routines  
688 that can be coupled with an EOS of readers' choice.

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**Supplementary Materials****On the stability and phase behavior of Titan's subsurface liquid columns**Sugata P. Tan<sup>1\*</sup>, Hertanto Adidharma<sup>2</sup><sup>1</sup>Planetary Science Institute, Tucson, AZ 85719, USA<sup>2</sup>Department of Petroleum Engineering, University of Wyoming, Laramie WY 82071, USA**A. Values plotted on the figures in the main paper****Table S1.** Values in Figure 2

| <b>Fig. 2a</b> |               |                             |                |                             | <b>Fig. 2b</b> |               |        |        |                |        |        |
|----------------|---------------|-----------------------------|----------------|-----------------------------|----------------|---------------|--------|--------|----------------|--------|--------|
| Depth [km]     | Low latitudes |                             | High latitudes |                             | Depth [km]     | Low latitudes |        |        | High latitudes |        |        |
|                | P [bar]       | $\rho$ [kg/m <sup>3</sup> ] | P [bar]        | $\rho$ [kg/m <sup>3</sup> ] |                | xN2           | xCH4   | xC2H6  | xN2            | xCH4   | xC2H6  |
| 0              | 1.467         | 596.08                      | 1.467          | 544.82                      | 0              | 0.0697        | 0.3673 | 0.5630 | 0.2039         | 0.7004 | 0.0957 |
| 1              | 9.503         | 592.71                      | 8.835          | 545.20                      | 1              | 0.0768        | 0.3769 | 0.5463 | 0.2202         | 0.6920 | 0.0878 |
| 2              | 17.494        | 589.34                      | 16.210         | 545.68                      | 2              | 0.0845        | 0.3863 | 0.5292 | 0.2371         | 0.6825 | 0.0804 |
| 3              | 25.439        | 585.98                      | 23.591         | 546.22                      | 3              | 0.0927        | 0.3953 | 0.5119 | 0.2544         | 0.6720 | 0.0736 |
| 4              | 33.338        | 582.64                      | 30.979         | 546.76                      | 4              | 0.1016        | 0.4041 | 0.4943 | 0.2721         | 0.6606 | 0.0672 |
| 5              | 41.193        | 579.31                      | 38.374         | 547.24                      | 5              | 0.1111        | 0.4124 | 0.4765 | 0.2902         | 0.6484 | 0.0614 |
| 6              | 49.003        | 575.99                      | 45.776         | 547.61                      | 6              | 0.1212        | 0.4202 | 0.4586 | 0.3084         | 0.6355 | 0.0561 |
| 7              | 56.768        | 572.68                      | 53.181         | 547.80                      | 7              | 0.1320        | 0.4276 | 0.4404 | 0.3267         | 0.6221 | 0.0512 |
| 8              | 64.488        | 569.38                      | 60.587         | 547.76                      | 8              | 0.1435        | 0.4344 | 0.4221 | 0.3450         | 0.6083 | 0.0467 |
| 9              | 72.163        | 566.08                      | 67.990         | 547.42                      | 9              | 0.1556        | 0.4406 | 0.4038 | 0.3632         | 0.5942 | 0.0426 |
| 10             | 79.794        | 562.77                      | 75.387         | 546.73                      | 10             | 0.1684        | 0.4461 | 0.3854 | 0.3812         | 0.5799 | 0.0389 |
| 11             | 87.380        | 559.42                      | 82.772         | 545.63                      | 11             | 0.1819        | 0.4510 | 0.3671 | 0.3988         | 0.5656 | 0.0355 |
| 12             | 94.920        | 556.03                      | 90.139         | 544.08                      | 12             | 0.1961        | 0.4551 | 0.3488 | 0.4161         | 0.5513 | 0.0325 |
| 13             | 102.415       | 552.57                      | 97.481         | 542.02                      | 13             | 0.2110        | 0.4584 | 0.3306 | 0.4330         | 0.5372 | 0.0298 |
| 14             | 109.861       | 549.00                      | 104.792        | 539.41                      | 14             | 0.2265        | 0.4609 | 0.3126 | 0.4494         | 0.5233 | 0.0273 |
| 15             | 117.259       | 545.28                      | 112.064        | 536.22                      | 15             | 0.2426        | 0.4625 | 0.2949 | 0.4653         | 0.5096 | 0.0251 |
| 16             | 124.604       | 541.38                      | 119.289        | 532.42                      | 16             | 0.2592        | 0.4633 | 0.2774 | 0.4806         | 0.4963 | 0.0231 |
| 17             | 131.896       | 537.22                      | 126.458        | 527.98                      | 17             | 0.2764        | 0.4632 | 0.2604 | 0.4953         | 0.4834 | 0.0213 |
| 18             | 139.129       | 532.76                      | 133.562        | 522.87                      | 18             | 0.2940        | 0.4622 | 0.2438 | 0.5094         | 0.4709 | 0.0197 |
| 19             | 146.300       | 527.92                      | 140.593        | 517.10                      | 19             | 0.3120        | 0.4603 | 0.2277 | 0.5229         | 0.4589 | 0.0182 |
| 20             | 153.402       | 522.62                      | 147.541        | 510.67                      | 20             | 0.3303        | 0.4575 | 0.2122 | 0.5357         | 0.4474 | 0.0169 |
| 21             | 160.429       | 516.80                      | 154.398        | 503.61                      | 21             | 0.3487        | 0.4539 | 0.1974 | 0.5479         | 0.4364 | 0.0158 |
| 22             | 167.373       | 510.37                      | 161.156        | 495.93                      | 22             | 0.3671        | 0.4496 | 0.1833 | 0.5594         | 0.4259 | 0.0147 |
| 23             | 174.226       | 503.27                      | 167.806        | 487.72                      | 23             | 0.3853        | 0.4446 | 0.1701 | 0.5701         | 0.4160 | 0.0138 |
| 24             | 180.978       | 495.46                      | 174.341        | 479.05                      | 24             | 0.4033        | 0.4390 | 0.1577 | 0.5802         | 0.4067 | 0.0130 |
| 25             | 187.619       | 486.93                      | 180.757        | 470.01                      | 25             | 0.4206        | 0.4330 | 0.1464 | 0.5897         | 0.3981 | 0.0123 |
| 26             | 194.141       | 477.72                      | 187.049        | 460.71                      | 26             | 0.4373        | 0.4266 | 0.1361 | 0.5984         | 0.3899 | 0.0117 |
| 27             | 200.534       | 467.91                      | 193.214        | 451.26                      | 27             | 0.4530        | 0.4202 | 0.1268 | 0.6065         | 0.3824 | 0.0111 |
| 28             | 206.791       | 457.66                      | 199.251        | 441.77                      | 28             | 0.4675        | 0.4137 | 0.1187 | 0.6139         | 0.3754 | 0.0106 |
| 29             | 212.907       | 447.12                      | 205.159        | 432.33                      | 29             | 0.4809        | 0.4075 | 0.1117 | 0.6208         | 0.3690 | 0.0102 |
| 30             | 218.880       | 436.48                      | 210.941        | 423.03                      | 30             | 0.4930        | 0.4014 | 0.1056 | 0.6271         | 0.3630 | 0.0099 |
| 31             | 224.710       | 425.90                      | 216.599        | 413.92                      | 31             | 0.5039        | 0.3957 | 0.1004 | 0.6330         | 0.3575 | 0.0096 |
| 32             | 230.397       | 415.51                      | 222.134        | 405.05                      | 32             | 0.5136        | 0.3904 | 0.0960 | 0.6384         | 0.3523 | 0.0093 |
| 33             | 235.946       | 405.40                      | 227.552        | 396.43                      | 33             | 0.5223        | 0.3854 | 0.0923 | 0.6434         | 0.3475 | 0.0090 |
| 34             | 241.360       | 395.62                      | 232.855        | 388.09                      | 34             | 0.5301        | 0.3808 | 0.0891 | 0.6481         | 0.3431 | 0.0088 |
| 35             | 246.645       | 386.22                      | 238.047        | 380.03                      | 35             | 0.5371        | 0.3764 | 0.0864 | 0.6525         | 0.3389 | 0.0086 |

**Table S2.** Values in Figure 3**Fig. 3a**

Low latitudes

| T [K] | curve<br>P [bar] | bubble<br>BP [bar] | dew<br>DP [bar] | upper dew<br>UDP [bar] |
|-------|------------------|--------------------|-----------------|------------------------|
| 94.0  | 1.467            | 1.467              |                 |                        |
| 96.3  | 9.503            |                    |                 |                        |
| 98.6  | 17.494           |                    |                 |                        |
| 100.9 | 25.439           |                    |                 |                        |
| 103.4 | 33.338           |                    |                 |                        |
| 105.8 | 41.193           |                    |                 |                        |
| 108.4 | 49.003           |                    |                 |                        |
| 111.0 | 56.768           |                    |                 |                        |
| 113.6 | 64.488           |                    |                 |                        |
| 116.3 | 72.163           |                    |                 |                        |
| 119.1 | 79.794           | 9.097              |                 |                        |
| 122.0 | 87.380           |                    |                 |                        |
| 124.9 | 94.920           |                    |                 |                        |
| 127.8 | 102.415          |                    |                 |                        |
| 130.9 | 109.861          |                    |                 |                        |
| 134.0 | 117.259          |                    |                 |                        |
| 137.2 | 124.604          |                    |                 |                        |
| 140.5 | 131.896          |                    |                 |                        |
| 143.8 | 139.129          |                    |                 |                        |
| 147.2 | 146.300          |                    |                 |                        |
| 150.7 | 153.402          | 38.847             |                 |                        |
| 154.3 | 160.429          |                    |                 |                        |
| 158.0 | 167.373          |                    |                 |                        |
| 161.7 | 174.226          |                    |                 |                        |
| 165.5 | 180.978          |                    |                 |                        |
| 169.4 | 187.619          | 69.711             |                 |                        |
| 173.5 | 194.141          | 76.199             |                 |                        |
| 177.6 | 200.534          | 81.669             | 5.687           |                        |
| 181.8 | 206.791          |                    | 7.920           | 85.5042                |
| 186.1 | 212.907          |                    | 11.006          | 87.2348                |
| 190.4 | 218.880          |                    | 15.328          | 86.587                 |
| 194.9 | 224.710          |                    | 21.592          | 83.2806                |
| 199.5 | 230.397          |                    | 31.602          | 76.0347                |
| 204.2 | 235.946          |                    |                 |                        |
| 209.1 | 241.360          |                    |                 |                        |
| 214.0 | 246.645          |                    |                 |                        |
| 219.0 | 251.805          |                    |                 |                        |
| 224.2 | 256.846          |                    |                 |                        |
| 229.4 | 261.772          |                    |                 |                        |
| 234.8 | 266.588          |                    |                 |                        |
| 240.3 | 271.300          |                    |                 |                        |
| 246.0 | 275.910          |                    |                 |                        |
| 251.7 | 280.423          |                    |                 |                        |
| 257.6 | 284.842          |                    |                 |                        |
| 263.7 | 289.172          |                    |                 |                        |
| 269.8 | 293.414          |                    |                 |                        |
| 276.2 | 297.573          |                    |                 |                        |
| 282.6 | 301.651          |                    |                 |                        |
| 289.2 | 305.650          |                    |                 |                        |
| 296.0 | 309.573          |                    |                 |                        |
| 302.9 | 313.422          |                    |                 |                        |

**Fig. 3b**

High latitudes

| T [K] | curve<br>P [bar] | bubble<br>BP [bar] | dew<br>DP [bar] | upper dew<br>UDP [bar] |
|-------|------------------|--------------------|-----------------|------------------------|
| 90.0  | 1.467            | 1.467              |                 |                        |
| 92.2  | 8.835            |                    |                 |                        |
| 94.4  | 16.210           |                    |                 |                        |
| 96.6  | 23.591           |                    |                 |                        |
| 99.0  | 30.979           |                    |                 |                        |
| 101.3 | 38.374           | 3.940              |                 |                        |
| 103.8 | 45.776           |                    |                 |                        |
| 106.3 | 53.181           |                    |                 |                        |
| 108.8 | 60.587           |                    |                 |                        |
| 111.4 | 67.990           |                    |                 |                        |
| 114.1 | 75.387           | 9.329              |                 |                        |
| 116.8 | 82.772           |                    |                 |                        |
| 119.6 | 90.139           |                    |                 |                        |
| 122.4 | 97.481           |                    |                 |                        |
| 125.4 | 104.792          |                    |                 |                        |
| 128.4 | 112.064          | 19.805             |                 |                        |
| 131.4 | 119.289          |                    |                 |                        |
| 134.5 | 126.458          |                    |                 |                        |
| 137.7 | 133.562          |                    |                 |                        |
| 141.0 | 140.593          |                    |                 |                        |
| 144.4 | 147.541          | 37.574             | 3.380           |                        |
| 147.8 | 154.398          | 41.865             | 5.021           |                        |
| 151.3 | 161.156          | 46.093             | 7.437           |                        |
| 154.9 | 167.806          | 49.857             | 11.041          |                        |
| 158.6 | 174.341          |                    | 16.620          | 52.442                 |
| 162.3 | 180.757          |                    | 26.269          | 52.009                 |
| 164.3 |                  |                    | 36.025          | 47.395                 |

**Table S3.** Values in Figure 4

| <b>Fig. 4a</b> |  | <b>Fig. 4b</b>  |            |
|----------------|--|---|------------|
| Depth [km]     | Low latitudes<br>P [bar] $\rho$ [kg/m <sup>3</sup> ] | High latitudes<br>P [bar] $\rho$ [kg/m <sup>3</sup> ] | Depth [km] |
| 0.0            | 1.467  | 596.08  | 0.0697     |
| 0.1            | 2.271  | 593.94  | 0.0728     |
| 0.2            | 3.073  | 591.81  | 0.0760     |
| 0.3            | 3.871  | 589.69  | 0.0792     |
| 0.4            | 4.667  | 587.59  | 0.0826     |
| 0.5            | 5.459  | 585.51  | 0.0859     |
| 0.6            | 6.249  | 583.43  | 0.0894     |
| 0.7            | 7.037  | 581.38  | 0.0929     |
| 0.8            | 7.821  | 579.33  | 0.0965     |
| 0.9            | 8.603  | 577.30  | 0.1001     |
| 1.0            | 9.382  | 575.28  | 0.1038     |
| 1.1            | 10.158   | 573.28  | 0.1075     |
| 1.2            | 10.931   | 571.28  | 0.1113     |
| 1.3            | 11.702   | 569.30  | 0.1152     |
| 1.4            | 12.470   | 567.33  | 0.1191     |
| 1.5            | 13.236   | 565.37  | 0.1231     |
| 1.6            | 13.999   | 563.41  | 0.1271     |
| 1.7            | 14.759   | 561.46  | 0.1312     |
| 1.8            | 15.516   | 559.52  | 0.1353     |
| 1.9            | 16.271   | 557.59  | 0.1394     |
| 2.0            | 17.024   | 555.66  | 0.1436     |
| 2.1            | 17.773   | 553.73  | 0.1479     |
| 2.2            | 18.521   | 551.80  | 0.1522     |
| 2.3            | 19.265   | 549.88  | 0.1565     |
| 2.4            | 20.007   | 547.95  | 0.1609     |
| 2.5            | 20.746   | 546.02  | 0.1653     |
| 2.6            | 21.483   | 544.08  | 0.1698     |
| 2.7            | 22.217   | 542.13  | 0.1743     |
| 2.8            | 22.949   | 540.18  | 0.1789     |
| 2.9            | 23.677   | 538.21  | 0.1835     |
| 3.0            | 24.404   | 536.23  | 0.1881     |
| 3.1            | 25.127   | 534.23  | 0.1928     |
| 3.2            | 25.848   | 532.21  | 0.1976     |
| 3.3            | 26.566   | 530.18  | 0.2024     |
| 3.4            | 27.281   | 528.11  | 0.2072     |
| 3.5            | 27.993   | 526.02  | 0.2121     |
| 3.6            | 28.703   | 523.90  | 0.2170     |
| 3.7            | 29.410   | 521.74  | 0.2220     |
| 3.8            | 30.113   | 519.54  | 0.2270     |
| 3.9            | 30.814   | 517.30  | 0.2321     |
| 4.0            | 31.512   | 515.01  | 0.2373     |
| 4.1            | 32.206   | 512.66  | 0.2425     |
| 4.2            | 32.898   | 510.26  | 0.2478     |
| 4.3            | 33.586   | 507.79  | 0.2532     |
| 4.4            | 34.270   | 505.25  | 0.2587     |
| 4.5            | 34.951   | 502.62  | 0.2643     |
| 4.6            | 35.629   | 499.90  | 0.2699     |
| 4.7            | 36.303   | 497.08  | 0.2757     |
| 4.8            | 36.973   | 494.15  | 0.2816     |
| 4.9            | 37.638   | 491.09  | 0.2877     |
| 5.0            | 38.300   | 487.88  | 0.2939     |
| 5.073          |  | 36.434  | 0.2939     |
| 5.1            | 38.957   | 484.5007  | 0.3003     |
| 5.2            | 39.610   | 480.9321  | 0.3069     |
| 5.3            | 40.257   | 477.1395  | 0.3138     |
| 5.4            | 40.899   | 473.0824  | 0.3210     |
| 5.5            | 41.536   | 468.7079  | 0.3285     |
| 5.643          | 42.435   | 461.7514  | 0.3402     |
|                |  | 425.89  | 0.5100     |
|                |  |   | 0.1498     |
|                |  | 5.073   | 0.4981     |
|                |  |   | 0.4897     |
|                |  | 5.1   | 0.3003     |
|                |  |   | 0.5158     |
|                |  | 5.2   | 0.3069     |
|                |  |   | 0.1839     |
|                |  | 5.3   | 0.3138     |
|                |  |   | 0.5152     |
|                |  | 5.4   | 0.3210     |
|                |  |   | 0.1779     |
|                |  | 5.5   | 0.3285     |
|                |  |   | 0.1718     |
|                |  | 5.643   | 0.3402     |
|                |  |   | 0.1656     |
|                |  | 5.5   | 0.3285     |
|                |  |   | 0.1592     |
|                |  | 5.643   | 0.3402     |
|                |  |   | 0.1498     |

**Table S4.** Values in Figure 5a**Fig. 5a**

| Bubble-point curve |        |        |        |        |        | Bubble- and dew-point curves |        |        | With three-phase VLL |        |        |
|--------------------|--------|--------|--------|--------|--------|------------------------------|--------|--------|----------------------|--------|--------|
| Depth              | 0      | km     | Depth  | 4      | km     | Depth                        | 5.64   | km     | Depth                | 2      | km     |
| xN2                | xCH4   | xC2H6  | xN2    | xCH4   | xC2H6  | xN2                          | xCH4   | xC2H6  | xN2                  | xCH4   | xC2H6  |
| 0.0396             | 0.0000 | 0.9604 | 0.2111 | 0.0000 | 0.7889 | 0.2031                       | 0.0000 | 0.7969 | 0.2275               | 0.0000 | 0.7725 |
| 0.0405             | 0.0163 | 0.9432 | 0.2143 | 0.0128 | 0.7729 | 0.2045                       | 0.0115 | 0.7839 | 0.2348               | 0.0142 | 0.7511 |
| 0.0426             | 0.0493 | 0.9082 | 0.2210 | 0.0386 | 0.7403 | 0.2075                       | 0.0348 | 0.7577 | 0.2507               | 0.0420 | 0.7073 |
| 0.0448             | 0.0828 | 0.8725 | 0.2283 | 0.0645 | 0.7071 | 0.2106                       | 0.0584 | 0.7310 | 0.2687               | 0.0691 | 0.6622 |
| 0.0471             | 0.1167 | 0.8362 | 0.2362 | 0.0905 | 0.6732 | 0.2139                       | 0.0822 | 0.7039 | 0.2894               | 0.0949 | 0.6157 |
| 0.0497             | 0.1511 | 0.7992 | 0.2448 | 0.1165 | 0.6386 | 0.2175                       | 0.1063 | 0.6762 | 0.3135               | 0.1191 | 0.5674 |
| 0.0524             | 0.1859 | 0.7617 | 0.2542 | 0.1424 | 0.6034 | 0.2214                       | 0.1307 | 0.6479 | 0.3421               | 0.1409 | 0.5170 |
| 0.0553             | 0.2210 | 0.7236 | 0.2644 | 0.1681 | 0.5674 | 0.2255                       | 0.1554 | 0.6190 | 0.3561               | 0.1486 | 0.4953 |
| 0.0585             | 0.2565 | 0.6851 | 0.2756 | 0.1935 | 0.5309 | 0.2300                       | 0.1804 | 0.5896 |                      |        |        |
| 0.0619             | 0.2921 | 0.6460 | 0.2878 | 0.2184 | 0.4938 | 0.2349                       | 0.2057 | 0.5594 |                      |        |        |
| 0.0655             | 0.3280 | 0.6066 | 0.3012 | 0.2426 | 0.4562 | 0.2401                       | 0.2313 | 0.5286 |                      |        |        |
| 0.0693             | 0.3639 | 0.5668 | 0.3158 | 0.2659 | 0.4183 | 0.2458                       | 0.2571 | 0.4972 |                      |        |        |
| 0.0734             | 0.3999 | 0.5267 | 0.3318 | 0.2880 | 0.3802 | 0.2520                       | 0.2831 | 0.4650 |                      |        |        |
| 0.0777             | 0.4358 | 0.4864 | 0.3492 | 0.3087 | 0.3421 | 0.2587                       | 0.3093 | 0.4320 |                      |        |        |
| 0.0824             | 0.4717 | 0.4460 | 0.3681 | 0.3275 | 0.3044 | 0.2661                       | 0.3355 | 0.3984 |                      |        |        |
| 0.0872             | 0.5073 | 0.4054 | 0.3885 | 0.3443 | 0.2672 | 0.2741                       | 0.3618 | 0.3641 |                      |        |        |
| 0.0924             | 0.5428 | 0.3649 | 0.4101 | 0.3589 | 0.2310 | 0.2829                       | 0.3881 | 0.3291 |                      |        |        |
| 0.0978             | 0.5779 | 0.3243 | 0.4327 | 0.3709 | 0.1963 | 0.2925                       | 0.4140 | 0.2934 |                      |        |        |
| 0.1035             | 0.6127 | 0.2838 | 0.4559 | 0.3806 | 0.1635 | 0.3031                       | 0.4396 | 0.2573 |                      |        |        |
| 0.1095             | 0.6470 | 0.2435 | 0.4789 | 0.3881 | 0.1330 | 0.3146                       | 0.4646 | 0.2208 |                      |        |        |
| 0.1158             | 0.6809 | 0.2033 | 0.5012 | 0.3938 | 0.1050 | 0.3273                       | 0.4886 | 0.1841 |                      |        |        |
| 0.1223             | 0.7143 | 0.1634 | 0.5220 | 0.3983 | 0.0797 | 0.3412                       | 0.5115 | 0.1474 |                      |        |        |
| 0.1292             | 0.7471 | 0.1237 | 0.5410 | 0.4020 | 0.0570 | 0.3563                       | 0.5328 | 0.1109 |                      |        |        |
| 0.1363             | 0.7794 | 0.0843 | 0.5577 | 0.4055 | 0.0368 | 0.3729                       | 0.5521 | 0.0750 |                      |        |        |
| 0.1437             | 0.8110 | 0.0453 | 0.5722 | 0.4091 | 0.0187 | 0.3914                       | 0.5687 | 0.0399 |                      |        |        |
| 0.1514             | 0.8420 | 0.0066 | 0.5843 | 0.4131 | 0.0026 | 0.4130                       | 0.5813 | 0.0057 |                      |        |        |
| 0.1527             | 0.8473 | 0.0000 | 0.5861 | 0.4139 | 0.0000 | 0.4172                       | 0.5828 | 0.0000 |                      |        |        |
| Depth              | 0.5    | km     |        |        |        | yN2                          | yCH4   | yC2H6  |                      |        |        |
| xN2                | xCH4   | xC2H6  |        |        |        | 0.9875                       | 0.0000 | 0.0125 | 0.3561               | 0.1486 | 0.4953 |
| 0.1318             | 0.0000 | 0.8682 |        |        |        | 0.9800                       | 0.0076 | 0.0125 | 0.3696               | 0.1629 | 0.4675 |
| 0.1362             | 0.0162 | 0.8475 |        |        |        | 0.9651                       | 0.0226 | 0.0123 | 0.3915               | 0.1824 | 0.4261 |
| 0.1458             | 0.0485 | 0.8057 |        |        |        | 0.9503                       | 0.0374 | 0.0122 | 0.4182               | 0.2008 | 0.3810 |
| 0.1563             | 0.0804 | 0.7633 |        |        |        | 0.9358                       | 0.0521 | 0.0121 | 0.4538               | 0.2172 | 0.3290 |
| 0.1679             | 0.1117 | 0.7204 |        |        |        | 0.9215                       | 0.0666 | 0.0120 | 0.5171               | 0.2284 | 0.2545 |
| 0.1807             | 0.1422 | 0.6771 |        |        |        | 0.9073                       | 0.0809 | 0.0118 | 0.5304               | 0.2284 | 0.2412 |
| 0.1949             | 0.1718 | 0.6333 |        |        |        | 0.8933                       | 0.0950 | 0.0117 | 0.5639               | 0.2233 | 0.2128 |
| 0.2106             | 0.2001 | 0.5893 |        |        |        | 0.8795                       | 0.1090 | 0.0115 | 0.5974               | 0.2182 | 0.1844 |
| 0.2282             | 0.2269 | 0.5449 |        |        |        | 0.8659                       | 0.1228 | 0.0113 | 0.6117               | 0.2142 | 0.1741 |
| 0.2478             | 0.2518 | 0.5004 |        |        |        | 0.8524                       | 0.1365 | 0.0112 | 0.6842               | 0.1859 | 0.1299 |
| 0.2698             | 0.2744 | 0.4558 |        |        |        | 0.8390                       | 0.1500 | 0.0110 | 0.7290               | 0.1629 | 0.1081 |
| 0.2945             | 0.2943 | 0.4112 |        |        |        | 0.8258                       | 0.1635 | 0.0108 | 0.7649               | 0.1421 | 0.0930 |
| 0.3224             | 0.3108 | 0.3668 |        |        |        | 0.8126                       | 0.1769 | 0.0105 | 0.7959               | 0.1227 | 0.0814 |
| 0.3537             | 0.3234 | 0.3228 |        |        |        | 0.7995                       | 0.1902 | 0.0103 | 0.8158               | 0.1095 | 0.0746 |
| 0.3888             | 0.3315 | 0.2797 |        |        |        | 0.7865                       | 0.2035 | 0.0100 |                      |        |        |
| 0.4272             | 0.3348 | 0.2380 |        |        |        | 0.7734                       | 0.2169 | 0.0097 |                      |        |        |
| 0.4675             | 0.3338 | 0.1988 |        |        |        | 0.7602                       | 0.2305 | 0.0094 |                      |        |        |
| 0.5072             | 0.3296 | 0.1632 |        |        |        | 0.7467                       | 0.2443 | 0.0090 |                      |        |        |
| 0.5436             | 0.3244 | 0.1320 |        |        |        | 0.7329                       | 0.2585 | 0.0086 |                      |        |        |
| 0.5751             | 0.3197 | 0.1052 |        |        |        | 0.7185                       | 0.2734 | 0.0081 |                      |        |        |
| 0.6013             | 0.3164 | 0.0823 |        |        |        | 0.7032                       | 0.2894 | 0.0074 |                      |        |        |
| 0.6229             | 0.3146 | 0.0625 |        |        |        | 0.6864                       | 0.3070 | 0.0066 |                      |        |        |
| 0.6406             | 0.3143 | 0.0450 |        |        |        | 0.6672                       | 0.3274 | 0.0055 |                      |        |        |
| 0.6553             | 0.3153 | 0.0294 |        |        |        | 0.6438                       | 0.3524 | 0.0038 |                      |        |        |
| 0.6675             | 0.3173 | 0.0152 |        |        |        | 0.6116                       | 0.3876 | 0.0008 |                      |        |        |
| 0.6776             | 0.3202 | 0.0021 |        |        |        | 0.6043                       | 0.3957 | 0.0000 |                      |        |        |
| 0.6792             | 0.3208 | 0.0000 |        |        |        |                              |        |        |                      |        |        |

**Table S5.** Values in Figure 5b**Fig. 5b**

| Bubble-point curve |        |        | Bubble- and dew-point curves |        |        | Two liquids (LL curve) |        |        |               |        |        |
|--------------------|--------|--------|------------------------------|--------|--------|------------------------|--------|--------|---------------|--------|--------|
| Depth 0 km         |        |        | Depth 5.07 km                |        |        | Depth 0.66 km          |        |        | Depth 1.95 km |        |        |
| xN2                | xCH4   | xC2H6  | xN2                          | xCH4   | xC2H6  | xN2                    | xCH4   | xC2H6  | xN2           | xCH4   | xC2H6  |
| 0.2406             | 0.7594 | 0.0000 | 0.5074                       | 0.4926 | 0.0000 | 0.1863                 | 0.0000 | 0.8137 | 0.2516        | 0.0000 | 0.7484 |
| 0.2366             | 0.7538 | 0.0096 | 0.4934                       | 0.4877 | 0.0189 | 0.1903                 | 0.0125 | 0.7972 | 0.2566        | 0.0123 | 0.7311 |
| 0.2288             | 0.7422 | 0.0290 | 0.4646                       | 0.4765 | 0.0589 | 0.1943                 | 0.0251 | 0.7806 | 0.2618        | 0.0246 | 0.7136 |
| 0.2211             | 0.7301 | 0.0488 | 0.4353                       | 0.4622 | 0.1024 | 0.1986                 | 0.0376 | 0.7638 | 0.2672        | 0.0368 | 0.6960 |
| 0.2134             | 0.7175 | 0.0691 | 0.4069                       | 0.4441 | 0.1490 | 0.2030                 | 0.0501 | 0.7469 | 0.2729        | 0.0490 | 0.6781 |
| 0.2060             | 0.7043 | 0.0897 | 0.3804                       | 0.4221 | 0.1975 | 0.2076                 | 0.0626 | 0.7299 | 0.2788        | 0.0611 | 0.6601 |
| 0.1987             | 0.6906 | 0.1108 | 0.3564                       | 0.3968 | 0.2468 | 0.2124                 | 0.0750 | 0.7126 | 0.2849        | 0.0731 | 0.6419 |
| 0.1915             | 0.6763 | 0.1322 | 0.3350                       | 0.3690 | 0.2960 | 0.2174                 | 0.0875 | 0.6952 | 0.2914        | 0.0851 | 0.6235 |
| 0.1846             | 0.6615 | 0.1539 | 0.3163                       | 0.3395 | 0.3442 | 0.2226                 | 0.0999 | 0.6775 | 0.2982        | 0.0970 | 0.6048 |
| 0.1778             | 0.6462 | 0.1760 | 0.2998                       | 0.3090 | 0.3912 | 0.2281                 | 0.1122 | 0.6597 | 0.3054        | 0.1089 | 0.5858 |
| 0.1712             | 0.6305 | 0.1983 | 0.2854                       | 0.2780 | 0.4366 | 0.2338                 | 0.1246 | 0.6416 | 0.3130        | 0.1206 | 0.5665 |
| 0.1648             | 0.6142 | 0.2210 | 0.2727                       | 0.2469 | 0.4804 | 0.2399                 | 0.1368 | 0.6233 | 0.3210        | 0.1322 | 0.5468 |
| 0.1586             | 0.5975 | 0.2439 | 0.2615                       | 0.2159 | 0.5225 | 0.2463                 | 0.1490 | 0.6047 | 0.3296        | 0.1437 | 0.5267 |
| 0.1526             | 0.5803 | 0.2671 | 0.2516                       | 0.1854 | 0.5630 | 0.2530                 | 0.1612 | 0.5858 | 0.3388        | 0.1551 | 0.5062 |
| 0.1467             | 0.5627 | 0.2906 | 0.2427                       | 0.1553 | 0.6020 | 0.2602                 | 0.1733 | 0.5665 | 0.3487        | 0.1663 | 0.4851 |
| 0.1411             | 0.5447 | 0.3142 | 0.2348                       | 0.1257 | 0.6395 | 0.2678                 | 0.1852 | 0.5469 | 0.3594        | 0.1773 | 0.4633 |
| 0.1356             | 0.5262 | 0.3381 | 0.2276                       | 0.0967 | 0.6757 | 0.2760                 | 0.1971 | 0.5269 | 0.3712        | 0.1880 | 0.4408 |
| 0.1304             | 0.5074 | 0.3622 | 0.2211                       | 0.0682 | 0.7107 | 0.2847                 | 0.2088 | 0.5064 | 0.3843        | 0.1985 | 0.4172 |
| 0.1253             | 0.4883 | 0.3865 | 0.2152                       | 0.0404 | 0.7444 | 0.2942                 | 0.2204 | 0.4854 | 0.3990        | 0.2086 | 0.3924 |
| 0.1203             | 0.4688 | 0.4109 | 0.2098                       | 0.0131 | 0.7771 | 0.3045                 | 0.2318 | 0.4637 | 0.4160        | 0.2183 | 0.3657 |
| 0.1156             | 0.4489 | 0.4355 | 0.2074                       | 0.0000 | 0.7926 | 0.3158                 | 0.2429 | 0.4413 | 0.4365        | 0.2272 | 0.3363 |
| 0.1110             | 0.4288 | 0.4602 |                              |        |        | 0.3283                 | 0.2538 | 0.4180 | 0.4631        | 0.2349 | 0.3020 |
| 0.1066             | 0.4083 | 0.4851 | yn2                          | yCH4   | yc2H6  | 0.3424                 | 0.2642 | 0.3934 | 0.5068        | 0.2396 | 0.2536 |
| 0.1023             | 0.3876 | 0.5101 | 0.7323                       | 0.2677 | 0.0000 | 0.3585                 | 0.2742 | 0.3673 | 0.5245        | 0.2391 | 0.2365 |
| 0.0982             | 0.3666 | 0.5352 | 0.7470                       | 0.2519 | 0.0011 | 0.3778                 | 0.2834 | 0.3389 | 0.5493        | 0.2352 | 0.2155 |
| 0.0943             | 0.3454 | 0.5603 | 0.7687                       | 0.2288 | 0.0024 | 0.4020                 | 0.2914 | 0.3066 | 0.5741        | 0.2314 | 0.1945 |
| 0.0905             | 0.3239 | 0.5856 | 0.7853                       | 0.2115 | 0.0032 | 0.4370                 | 0.2970 | 0.2660 | 0.5928        | 0.2264 | 0.1808 |
| 0.0868             | 0.3023 | 0.6109 | 0.7993                       | 0.1970 | 0.0037 | 0.4471                 | 0.2975 | 0.2554 | 0.6418        | 0.2089 | 0.1492 |
| 0.0833             | 0.2804 | 0.6363 | 0.8120                       | 0.1839 | 0.0041 | 0.4531                 | 0.2975 | 0.2494 | 0.6736        | 0.1946 | 0.1317 |
| 0.0800             | 0.2583 | 0.6617 | 0.8239                       | 0.1716 | 0.0044 | 0.4599                 | 0.2974 | 0.2427 | 0.6993        | 0.1816 | 0.1191 |
| 0.0767             | 0.2361 | 0.6872 | 0.8357                       | 0.1596 | 0.0047 | 0.5000                 | 0.2950 | 0.2050 | 0.7216        | 0.1694 | 0.1090 |
| 0.0736             | 0.2137 | 0.7127 | 0.8474                       | 0.1477 | 0.0049 | 0.5447                 | 0.2812 | 0.1742 | 0.7415        | 0.1578 | 0.1007 |
| 0.0707             | 0.1911 | 0.7382 | 0.8591                       | 0.1357 | 0.0051 | 0.5521                 | 0.2787 | 0.1692 | 0.7598        | 0.1467 | 0.0936 |
| 0.0678             | 0.1685 | 0.7637 | 0.8711                       | 0.1236 | 0.0053 | 0.5586                 | 0.2764 | 0.1651 | 0.7767        | 0.1359 | 0.0874 |
| 0.0651             | 0.1457 | 0.7892 | 0.8832                       | 0.1114 | 0.0055 | 0.5698                 | 0.2721 | 0.1581 | 0.7926        | 0.1255 | 0.0819 |
| 0.0625             | 0.1228 | 0.8148 | 0.8955                       | 0.0989 | 0.0056 | 0.6105                 | 0.2543 | 0.1353 | 0.8077        | 0.1153 | 0.0770 |
| 0.0600             | 0.0998 | 0.8402 | 0.9080                       | 0.0863 | 0.0057 | 0.6403                 | 0.2390 | 0.1207 | 0.8220        | 0.1054 | 0.0726 |
| 0.0576             | 0.0767 | 0.8657 | 0.9207                       | 0.0735 | 0.0059 | 0.6651                 | 0.2251 | 0.1098 | 0.8357        | 0.0957 | 0.0686 |
| 0.0553             | 0.0536 | 0.8911 | 0.9335                       | 0.0605 | 0.0060 | 0.6869                 | 0.2121 | 0.1010 | 0.8489        | 0.0863 | 0.0649 |
| 0.0531             | 0.0304 | 0.9165 | 0.9466                       | 0.0473 | 0.0061 | 0.7066                 | 0.1997 | 0.0937 | 0.8615        | 0.0770 | 0.0615 |
| 0.0510             | 0.0071 | 0.9419 | 0.9599                       | 0.0339 | 0.0062 | 0.7247                 | 0.1879 | 0.0874 | 0.8738        | 0.0679 | 0.0583 |
| 0.0504             | 0.0000 | 0.9496 | 0.9733                       | 0.0204 | 0.0063 | 0.7416                 | 0.1764 | 0.0820 | 0.8857        | 0.0589 | 0.0554 |
|                    |        |        | 0.9869                       | 0.0067 | 0.0064 | 0.7575                 | 0.1654 | 0.0771 | 0.8972        | 0.0501 | 0.0527 |
| Depth 4 km         |        |        | 0.9936                       | 0.0000 | 0.0064 | 0.7726                 | 0.1547 | 0.0728 | 0.9084        | 0.0415 | 0.0502 |
| xN2                |        |        |                              |        |        | 0.7869                 | 0.1442 | 0.0688 | 0.9193        | 0.0329 | 0.0478 |
| 0.6599             | 0.3401 | 0.0000 |                              |        |        | 0.8007                 | 0.1340 | 0.0653 | 0.9299        | 0.0245 | 0.0456 |
| 0.6455             | 0.3348 | 0.0197 |                              |        |        | 0.8140                 | 0.1241 | 0.0620 | 0.9403        | 0.0162 | 0.0435 |
| 0.6047             | 0.3299 | 0.0654 |                              |        |        | 0.8268                 | 0.1143 | 0.0590 | 0.9505        | 0.0081 | 0.0415 |
| 0.5458             | 0.3280 | 0.1262 |                              |        |        | 0.8391                 | 0.1047 | 0.0562 | 0.9604        | 0.0000 | 0.0396 |
| 0.4759             | 0.3196 | 0.2045 |                              |        |        | 0.8511                 | 0.0953 | 0.0536 |               |        |        |
| 0.4121             | 0.2969 | 0.2910 |                              |        |        | 0.8628                 | 0.0860 | 0.0512 |               |        |        |
| 0.3623             | 0.2627 | 0.3751 |                              |        |        | 0.8742                 | 0.0769 | 0.0489 |               |        |        |
| 0.3247             | 0.2228 | 0.4524 |                              |        |        | 0.8853                 | 0.0679 | 0.0468 |               |        |        |
| 0.2960             | 0.1813 | 0.5227 |                              |        |        | 0.8961                 | 0.0590 | 0.0449 |               |        |        |
| 0.2734             | 0.1399 | 0.5867 |                              |        |        | 0.9067                 | 0.0503 | 0.0430 |               |        |        |
| 0.2552             | 0.0996 | 0.6453 |                              |        |        | 0.9171                 | 0.0417 | 0.0412 |               |        |        |
| 0.2401             | 0.0607 | 0.6992 |                              |        |        | 0.9273                 | 0.0331 | 0.0396 |               |        |        |
| 0.2275             | 0.0233 | 0.7493 |                              |        |        | 0.9373                 | 0.0247 | 0.0380 |               |        |        |
| 0.2203             | 0.0000 | 0.7797 |                              |        |        | 0.9471                 | 0.0164 | 0.0365 |               |        |        |
|                    |        |        |                              |        |        | 0.9567                 | 0.0082 | 0.0351 |               |        |        |
|                    |        |        |                              |        |        | 0.9662                 | 0.0000 | 0.0338 |               |        |        |

**Table S6.** Values in Figure 6**Fig. 6a**

| Depth<br>[km] | Low latitudes           |                        |                      | High latitudes         |                      |
|---------------|-------------------------|------------------------|----------------------|------------------------|----------------------|
|               | Lithospheric<br>P [bar] | Hydrostatic<br>P [bar] | Capillary<br>P [bar] | Hydrostatic<br>P [bar] | Capillary<br>P [bar] |
| 0             | 0.000                   | 1.467                  | 345.580              | 1.467                  | 222.518              |
| 1             | 12.628                  | 9.503                  | 337.601              | 8.835                  | 215.784              |
| 2             | 25.255                  | 17.494                 | 329.530              | 16.210                 | 208.976              |
| 3             | 37.883                  | 25.439                 | 321.366              | 23.591                 | 202.060              |
| 4             | 50.511                  | 33.338                 | 313.107              | 30.979                 | 194.994              |
| 5             | 63.138                  | 41.193                 | 304.743              | 38.374                 | 187.728              |
| 6             | 75.766                  | 49.003                 | 296.265              | 45.776                 | 180.200              |
| 7             | 88.394                  | 56.768                 | 287.656              | 53.181                 | 172.333              |
| 8             | 101.021                 | 64.488                 | 278.894              | 60.587                 | 164.033              |
| 9             | 113.649                 | 72.163                 | 269.950              | 67.990                 | 155.183              |
| 10            | 126.277                 | 79.794                 | 260.780              | 75.387                 | 145.634              |
| 11            | 138.904                 | 87.380                 | 251.327              | 82.772                 | 135.205              |
| 12            | 151.532                 | 94.920                 | 241.506              | 90.139                 | 123.672              |
| 13            | 164.160                 | 102.415                | 231.197              | 97.481                 | 110.781              |
| 14            | 176.788                 | 109.861                | 220.218              | 104.792                | 96.288               |
| 15            | 189.415                 | 117.259                | 208.296              | 112.064                | 80.080               |
| 15.384        |                         |                        |                      | 73.438                 |                      |
| 16            | 202.043                 | 124.604                | 194.996              | 119.289                |                      |
| 17            | 214.671                 | 131.896                | 179.625              | 126.458                |                      |
| 18            | 227.298                 | 139.129                | 161.081              | 133.562                |                      |
| 19            | 239.926                 | 146.300                | 137.732              | 140.593                |                      |
| 19.143        |                         | 133.893                |                      | 174.341                |                      |
| 20            | 252.554                 | 153.402                |                      | 147.541                |                      |
| 21            | 265.181                 | 160.429                |                      | 154.398                |                      |
| 22            | 277.809                 | 167.373                |                      | 161.156                |                      |
| 23            | 290.437                 | 174.226                |                      | 167.806                |                      |
| 24            | 303.064                 | 180.978                |                      | 174.341                |                      |
| 25            | 315.692                 | 187.619                |                      |                        |                      |
| 26            | 328.320                 | 194.141                |                      |                        |                      |
| 27            | 340.947                 | 200.534                |                      |                        |                      |
| 28            | 353.575                 | 206.791                |                      |                        |                      |

**Fig. 6b**

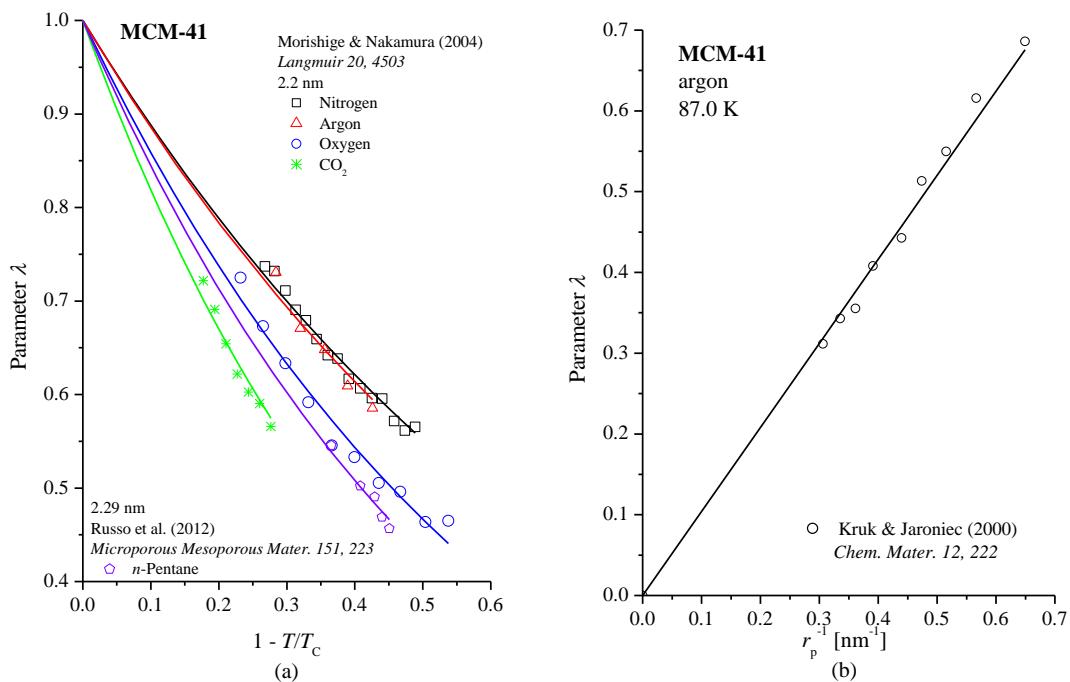
| Depth<br>[km] | Low latitudes           |                        |                      | High latitudes         |                      |
|---------------|-------------------------|------------------------|----------------------|------------------------|----------------------|
|               | Lithospheric<br>P [bar] | Hydrostatic<br>P [bar] | Capillary<br>P [bar] | Hydrostatic<br>P [bar] | Capillary<br>P [bar] |
| 0.00          | 0.000                   | 1.467                  | 345.580              | 1.467                  | 222.518              |
| 0.10          | 1.203                   | 2.271                  | 341.385              | 2.203                  | 219.177              |
| 0.20          | 2.407                   | 3.073                  | 337.210              | 2.938                  | 215.874              |
| 0.30          | 3.610                   | 3.871                  | 333.064              | 3.672                  | 212.613              |
| 0.40          | 4.813                   | 4.667                  | 328.948              | 4.405                  | 209.388              |
| 0.50          | 6.016                   | 5.459                  | 324.862              | 5.137                  | 206.194              |
| 0.60          | 7.220                   | 6.249                  | 320.804              | 5.868                  | 203.025              |
| 0.70          | 8.423                   | 7.037                  | 316.775              | 6.598                  | 199.876              |
| 0.80          | 9.626                   | 7.821                  | 312.775              | 7.327                  | 196.742              |
| 0.90          | 10.830                  | 8.603                  | 308.801              | 8.055                  | 193.618              |
| 1.00          | 12.033                  | 9.382                  | 304.854              | 8.782                  | 190.498              |
| 1.10          | 13.236                  | 10.158                 | 300.933              | 9.508                  | 187.378              |
| 1.20          | 14.439                  | 10.931                 | 297.035              | 10.233                 | 184.251              |
| 1.30          | 15.643                  | 11.702                 | 293.161              | 10.957                 | 181.113              |
| 1.40          | 16.846                  | 12.470                 | 289.308              | 11.679                 | 177.958              |
| 1.50          | 18.049                  | 13.236                 | 285.475              | 12.400                 | 174.781              |
| 1.60          | 19.252                  | 13.999                 | 281.660              | 13.120                 | 171.575              |
| 1.70          | 20.456                  | 14.759                 | 277.861              | 13.838                 | 168.335              |
| 1.80          | 21.659                  | 15.516                 | 274.076              | 14.555                 | 165.054              |
| 1.90          | 22.862                  | 16.271                 | 270.302              | 15.270                 | 161.727              |
| 2.00          | 24.066                  | 17.024                 | 266.538              | 15.984                 | 158.345              |
| 2.10          | 25.269                  | 17.773                 | 262.780              | 16.696                 | 154.901              |
| 2.20          | 26.472                  | 18.521                 | 259.024              | 17.406                 | 151.389              |
| 2.30          | 27.675                  | 19.265                 | 255.269              | 18.115                 | 147.799              |
| 2.40          | 28.879                  | 20.007                 | 251.510              | 18.821                 | 144.124              |
| 2.50          | 30.082                  | 20.746                 | 247.743              | 19.526                 | 140.354              |
| 2.60          | 31.285                  | 21.483                 | 243.963              | 20.228                 | 136.479              |
| 2.70          | 32.489                  | 22.217                 | 240.166              | 20.928                 | 132.489              |
| 2.80          | 33.692                  | 22.949                 | 236.347              | 21.626                 | 128.374              |
| 2.90          | 34.895                  | 23.677                 | 232.499              | 22.321                 | 124.122              |
| 3.00          | 36.098                  | 24.404                 | 228.616              | 23.013                 | 119.722              |
| 3.10          | 37.302                  | 25.127                 | 224.690              | 23.703                 | 115.162              |
| 3.20          | 38.505                  | 25.848                 | 220.713              | 24.390                 | 110.430              |
| 3.30          | 39.708                  | 26.566                 | 216.675              | 25.074                 | 105.516              |
| 3.40          | 40.912                  | 27.281                 | 212.567              | 25.755                 | 100.410              |
| 3.50          | 42.115                  | 27.993                 | 208.375              | 26.432                 | 95.106               |
| 3.60          | 43.318                  | 28.703                 | 204.087              | 27.106                 | 89.598               |
| 3.70          | 44.521                  | 29.410                 | 199.686              | 27.776                 | 83.890               |
| 3.80          | 45.725                  | 30.113                 | 195.156              | 28.442                 | 77.989               |
| 3.879         |                         |                        |                      | 73.202                 |                      |
| 3.90          | 46.928                  | 30.814                 | 190.475              | 29.104                 |                      |
| 4.00          | 48.131                  | 31.512                 | 185.620              | 29.762                 |                      |
| 4.10          | 49.334                  | 32.206                 | 180.564              | 30.415                 |                      |
| 4.20          | 50.538                  | 32.898                 | 175.276              | 31.062                 |                      |
| 4.30          | 51.741                  | 33.586                 | 169.721              | 31.705                 |                      |
| 4.40          | 52.944                  | 34.270                 | 163.857              | 32.341                 |                      |
| 4.50          | 54.148                  | 34.951                 | 157.641              | 32.972                 |                      |
| 4.60          | 55.351                  | 35.629                 | 151.019              | 33.596                 |                      |
| 4.70          | 56.554                  | 36.303                 | 143.936              | 34.212                 |                      |
| 4.80          | 57.757                  | 36.973                 | 136.334              | 34.821                 |                      |
| 4.90          | 58.961                  | 37.638                 | 128.152              | 35.421                 |                      |
| 5.00          | 60.164                  | 38.300                 | 119.340              | 36.010                 |                      |
| 5.017         |                         |                        | 117.777              |                        |                      |
| 5.073         |                         |                        |                      | 36.434                 |                      |
| 5.10          | 61.367                  | 38.957                 |                      |                        |                      |
| 5.20          | 62.571                  | 39.610                 |                      |                        |                      |
| 5.30          | 63.774                  | 40.257                 |                      |                        |                      |
| 5.40          | 64.977                  | 40.899                 |                      |                        |                      |
| 5.50          | 66.180                  | 41.536                 |                      |                        |                      |
| 5.643         | 67.901                  | 42.435                 |                      |                        |                      |

**Table S7.** Values in Figure A1**Fig. A1**

| Depth<br>[km] | High Latitudes |        | [mW/m <sup>2</sup> ] |
|---------------|----------------|--------|----------------------|
|               | q =<br>13.8    | 5.4    |                      |
| 0             | 90.00          | 90.00  |                      |
| 1             | 92.16          | 100.84 |                      |
| 2             | 94.38          | 111.69 |                      |
| 3             | 96.64          | 122.54 |                      |
| 4             | 98.96          | 133.39 |                      |
| 5             | 101.34         | 144.24 |                      |
| 6             | 103.77         | 155.09 |                      |
| 7             | 106.25         |        |                      |
| 8             | 108.80         |        |                      |
| 9             | 111.40         |        |                      |
| 10            | 114.07         |        |                      |
| 11            | 116.79         |        |                      |
| 12            | 119.58         |        |                      |
| 13            | 122.44         |        |                      |
| 14            | 125.36         |        |                      |
| 15            | 128.35         |        |                      |
| 16            | 131.41         |        |                      |
| 17            | 134.54         |        |                      |
| 18            | 137.74         |        |                      |
| 19            | 141.02         |        |                      |
| 20            | 144.37         |        |                      |
| 21            | 147.80         |        |                      |
| 22            | 151.31         |        |                      |
| 23            | 154.91         |        |                      |
| 24            | 158.58         |        |                      |
| 25            | 162.34         |        |                      |
| 26            | 166.19         |        |                      |
| 27            | 170.12         |        |                      |
| 28            | 174.15         |        |                      |
| 29            | 178.27         |        |                      |
| 30            | 182.48         |        |                      |
| 31            | 186.79         |        |                      |
| 32            | 191.20         |        |                      |
| 33            | 195.71         |        |                      |
| 34            | 200.33         |        |                      |
| 35            | 205.05         |        |                      |

## B. Derivation procedure of $\lambda$ parameters

The exponential behavior of parameter  $\lambda$  with temperature as stated in Eq (A9) in the main paper can be traced to the observation over experimentally derived values shown in Fig. S1(a) for various confined fluids in MCM-41 porous medium. Also note that the parameter is unity at the bulk critical temperature. Moreover, the parameter behaves linearly with respect to the reciprocal of pore radius as shown in panel (b), which also include the origin to represent the free bulk phase where the capillary pressure vanishes; the parameter is also zero at the origin as there is no capillary effect in the bulk.



**Figure S1.** The behavior of parameter  $\lambda$  from literature with respect to: (a) temperature; (b) pore radius. The parameter's values are derived from experimental capillary-condensation data as in Tan & Piri (Fluid Phase Equilib. 2015, 393, 48).

These behaviors enable us to estimate, to a first approximation, the parameter of a confined fluid as long as there is at least a data value available. We apply the linearity to estimate the parameter if the data is only available for pores of a different but similar size, and then use the exponential to get the coefficient  $A_i$  in Eq (A9). For nitrogen, the data in Figure S1 is directly used. However, there is no data for methane and ethane in 2.2-nm MCM-41. Therefore, the estimation as described above is used for these two components. Our measured data of methane at 123.4 K and 126.4 K in 1.77-nm MCM-41 (Yang et al., 2022, Langmuir, accepted), and ethane at pore critical temperature of 225.9 K in 2.1-nm MCM-41 (Tan et al., Ind. Eng. Chem. Res. 2020, 59, 10673) are used for the estimation. For the record, as all data of ethane are supercritical in 2.1-nm MCM-41, the pore critical temperature is calculated by extrapolation down to cross the spinodal. As stated in the main paper, the resulting coefficients  $A_i$  are listed in Table 3.

### C. Subroutine codes for thermo-gravitational effects

The codes were written in FORTRAN and had been tested and run for the calculations using Compaq Visual Fortran © 2000 Professional Edition 6.6.0. The routines to calculate the fugacity coefficients and density, which depend on the users' choice of EOS, as well as that calculates the inverse of a matrix, are not included, so they need to be provided by the users.

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```
!-----
! Program package
! Thermo-gravitational effects: Titan's subsurface liquids
! Written by: Sugata Tan - 2021
! Funded by NASA SSW Grant 80NSSC19K0792
!
! Two subroutines that are equation of state (EOS) specific, to be used with EOS chosen by users,
! are not provided here:
!     (1) DENSITY      -      to calculate the density of a phase at T, P, and composition
!     (2) FCOEF        -      to calculate the fugacity coefficient of a phase at T, P, and
!                           composition
!
! A subroutine to calculate the inverse of an (N x N) matrix is not provided here
!     INVERSE(A,N,D) - to calculate the inverse of matrix A of dimension (N x N); the outputs
!                       are the inverse A and determinant D
!-----
! Defining variables universally used across the main program and its subroutines
!
MODULE universal_vars
    IMPLICIT NONE
    DOUBLE PRECISION :: P0, dh, dT, grav, R, pi
    DOUBLE PRECISION, DIMENSION(:), ALLOCATABLE :: molWt
    INTEGER :: nComp
!
END MODULE universal_vars
!-----
! The main program
!
PROGRAM Thermograv
    USE universal_vars
!
    PARAMETER (nC = 3)      ! Titan's fluid is assumed to be a ternary mixture of
                           ! N2(1)/CH4(2)/C2H6(3)
    DOUBLE PRECISION :: MW(nC), Z0_0(nC), Z0_1(nC), Z0_2(nC), Z(nC), X(nC), Y(nC)
    DOUBLE PRECISION :: T0, q, rho
    DOUBLE PRECISION :: h, hmin, hmax, T, TL, TU, P
    INTEGER :: lit, i, n
```

```

nComp = nC
ALLOCATE(molWt(nComp))
R = 83.1447d0           ! Gas constant in [bar.cc/mol/K]

! Titan's fluid; the parameters of pure components depend on the equation of state in use
! (not included here)

DATA MW /28.018d0, 16.043d0, 30.07d0/           ! The molecular weights of the components:
! N2, CH4, C2H6
! The composition at surface in equilibrium with the atmosphere in low latitudes

DATA z0_0 /0.069676714d0, 0.367302904d0, 0.563020382d0/

! The composition at surface in equilibrium with the atmosphere in high latitudes

DATA z0_1 /0.203892325d0, 0.700433111d0, 0.095674565d0/

! Titan

grav = 1.352d0           ! [m/s2]      gravity
P0 = 1.467d0             ! [bar]        pressure at the surface
molWt = MW                ! molecular weight of the components

! Cases (the value in the last order is the active one for calculation, swap for the desired case)

lit = 0                  ! subsurface liquid in water-ice crust in low latitudes
lit = 1                  ! subsurface liquid in water-ice crust in high latitudes
lit = 2                  ! subsurface liquid in methane-clathrate crust in low latitudes
lit = 3                  ! subsurface liquid in methane-clathrate crust in high latitudes

! Layering

hmin = 0.d0              ! from the surface
dh = -1.d0                ! [meter]      depth increment set to be 1 meter

SELECT CASE (lit)

    CASE (0)           ! subsurface liquid in water-ice crust in low latitudes
        T0 = 94.d0      ! [K]          temperature of surface in low latitudes
        Z = z0_0
        hmax = -3.5d4  ! [meter]     maximum depth of 35 km
        q = 13.8d-3    ! [W/m2]      heat flux

    CASE (1)           ! subsurface liquid in water-ice crust in high latitudes
        T0 = 90.d0      ! [K]          temperature of surface in low latitudes
        Z = z0_1
        hmax = -3.5d4  ! [meter]     maximum depth of 35 km
        q = 13.8d-3    ! [W/m2]      heat flux

    CASE (2)           ! subsurface liquid in CH4-clathrate crust in low latitudes
        T0 = 94.d0      ! [K]          temperature of surface in low latitudes
        Z = z0_0
        hmax = -6.d3   ! [meter]     maximum depth of 6 km
        q = 5.425d-3   ! [W/m2]      heat flux

    CASE (3)           ! subsurface liquid in CH4-clathrate in high latitudes
        T0 = 90.d0      ! [K]          temperature of surface in high latitudes
        Z = z0_1
        hmax = -6.d3   ! [meter]     maximum depth of 6 km
        q = 5.425d-3   ! [W/m2]      heat flux

END SELECT

OPEN(2,file='results.txt')    ! Opening a text file to record the results

! Calculating property profiles of subsurface liquids from hmin to hmax

```

```

X = Z; Y = Z                                ! Initial guess for the composition at the layer boundaries
DO h = hmin, hmax, dh
    ht = h+dh/2.d0                         ! the middle point of a layer
    ! Temperature profile obtained from Eq (A1)
    IF (lit > 1) THEN          ! methane-clathrate crust
        T = T0-q*ht/0.5d0
        TL = T0-q*h/0.5d0
        TU = T0-q*(h+dh)/0.5d0
        n = 100
    ELSE          ! water-ice crust
        T = (T0**0.0248d0-0.0248d0*ht*q/10.d0**2.7154d0)**(1.d0/0.0248d0)
        TL = (T0**0.0248d0-0.0248d0*h*q/10.d0**2.7154d0)**(1.d0/0.0248d0)
        TU = (T0**0.0248d0-0.0248d0*(h+dh)*q/10.d0**2.7154d0)**(1.d0/0.0248d0)
        n = 1000
    END IF
    ! Calculate the pressure, density, and composition profiles
    dT = TU-TL      ! Temperature increment between lower and upper boundaries of layer
    ! EOS-specific subroutine, using EOS chosen by user, not provided here
    CALL DENSITY(1,P0,T,Z,rho)
    ! Initial value to start the calculation of pressure gradient
    P = P0-rho*sum(z*MW)*grav*dh*1.d-2
    ! Calculate the pressure [bar] and composition Y at the depth of h
    CALL P_COMP(T,P,Z,X,Y)
    ! Calculate the density in [mol/cc] at the depth of h
    CALL DENSITY(1,P,T,Y,rho)
    rho = rho*sum(Y*MW)*1.d3      ! Convert to the unit of [kg/m3]
    ! At this point, X = Z is the composition of the upper boundary and Y is of the
    ! lower boundary of the layer
    ! Print out the results and store in the output file every n meters of depth
    i = INT(h); i = ABS(i)
    IF(MOD(i,n) == (n+INT(dh))) THEN
        WRITE(2,"(X,F9.2,2(2X,F10.5),3X,3(F15.9,3X),F9.4)") DABS(h+dh), T, P, &
            &Y(1), Y(2), Y(3), rho
        PRINT*, DABS(h+dh)      ! For display on screen
    END IF
    ! Updating for the next iteration
    Z = Y
    Y = X
    P0 = P
END DO
STOP

END PROGRAM Thermograv
!-----
! Subroutine to calculate pressure and composition due to thermo-gravitational effects using the
! algorithm for bubble points at T and Z (see the main paper)
SUBROUTINE P_COMP(T,P,Z,X,Y)
    USE universal_vars
    IMPLICIT NONE
    DOUBLE PRECISION, INTENT(IN) :: T, Z(nComp)
    DOUBLE PRECISION, INTENT(INOUT) :: P, X(nComp), Y(nComp)
    DOUBLE PRECISION :: YY(nComp), K(nComp), KK(nComp), dK_dP(nComp), dK_dY(nComp,nComp)
    DOUBLE PRECISION :: diff, det, delta(nComp+1), func(nComp+1), jac(nComp+1,nComp+1)
    INTEGER :: i, j

```

```

! Newton-Raphson method to solve the phase-equilibrium equations

diff = 1.d-4; det=1.d0
X = Z
DO WHILE (det.gt.1.0D-10)

! Calculate K factors

    CALL KFACT(P,T,X,Y,K)

! Calculate derivative of K factor with respect to composition (mol fraction)

    YY = Y
    DO i = 1,nComp
        DO j = 1,nComp
            YY(j)=Y(j)*(1.d0+diff)
            CALL KFACT(P,T,X,YY,KK)
            YY=Y
            dK_dY(i,j) = (KK(i)-K(i))/(diff*Y(j))
        END DO
    END DO

! Calculate derivative of K factor with respect to P or T

    CALL KFACT(P*(1.d0+diff),T,X,Y,KK)
    dK_dP = (KK-K)/(diff*P)

! The zero functions

    DO i = 1,nComp
        func(i) = -Y(i)+K(i)*Z(i)      ! energy balance (equifugacity)
    END DO
    func(nComp+1) = -1.d0+SUM(Y)      ! consistency equation

! Build the Jacobian for bubble-point calculations

    DO i = 1,nComp
        DO j=1,nComp
            jac(i,j) = Z(i)*dK_dY(i,j)
        END DO
        jac(i,i) = jac(i,i)-1.0D0
        jac(i,nComp+1)=Z(i)*dK_dP(i)
        jac(nComp+1,i)= 1.d0
    END DO
    jac(nComp+1,nComp+1) = 0.0D0

! Using inverse of Jacobian to solve the linear equations

    CALL INVERSE(jac,nComp+1,det)      ! The INVERSE subroutine is not included

    delta = 0.d0
    DO i = 1,nComp+1
        DO j = 1,nComp+1
            delta(i) = delta(i)+jac(i,j)*func(j)
        END DO
    END DO

    det = 0.d0
    DO i = 1,nComp+1
        det = det + delta(i)**2
    END DO
    det = DSQRT(det/(nComp+1))

! Updating the variables

    P = P-delta(nComp+1)
    Y = Y-delta(1:nComp)

    END DO

END SUBROUTINE P_COMP

```

```

!-----
! Subroutine to calculate the K-factor at P, T, X, Y
! Originally, it is for vapor-liquid equilibria, but now modified for thermo-gravity purposes

SUBROUTINE KFACT(P,T,X,Y,K)

    USE universal_vars

    IMPLICIT NONE
    DOUBLE PRECISION, INTENT(IN) :: P, T, X(nComp), Y(nComp)
    DOUBLE PRECISION, INTENT(OUT) :: K(nComp)
    DOUBLE PRECISION :: ln_fugacityCoef_v(nComp)
    DOUBLE PRECISION :: ln_fugacityCoef_l(nComp), Qnet(nComp)
    INTEGER :: phase

    phase = 1      ! For common vapor-liquid equilibria, change to vapor phase (phase = 0)

! EOS-specific subroutine to calculate phase fugacity coefficient (not provided here)

    CALL FCOEF(phase,P,T,Y,ln_fugacityCoef_v)
    CALL FCOEF(1,P0,T,X,ln_fugacityCoef_l)

! Calculate K-factor

    K = DEXP(ln_fugacityCoef_l-ln_fugacityCoef_v)

! Inclusion of thermo-gravitational effects

    CALL Qdiff(1,P,T,Y,Qnet)      ! Thermal diffusion in subsurface liquid at P, T, Y
    K = K*dexp(-molWt*1.d-2*grav*(dh)/R/T-Qnet/T*dT)*P0/P

END SUBROUTINE KFACT

!-----
! Subroutine to calculate the net heat diffusion in a phase at P, T, X
! Based on Firoozabadi et al. (2000)

SUBROUTINE Qdiff(phase,P,T,X,Qnet)

    USE universal_vars
    IMPLICIT NONE
    DOUBLE PRECISION, INTENT(IN) :: P, T, X(nComp)
    DOUBLE PRECISION, INTENT(OUT) :: Qnet(nComp)
    INTEGER, INTENT(IN) :: phase
    DOUBLE PRECISION :: V(nComp), H(nComp), rho, rho1, rho2, ln_fugacityCoef(nComp)
    DOUBLE PRECISION :: d_lnPhi_dP(nComp), d_lnPhi_dT(nComp), U(nComp)

! Calculate the partial molar volume

    CALL FCOEF(phase,P*1.0001d0,T,X,ln_fugacityCoef)
    CALL FCOEF(phase,P*0.9999d0,T,X,d_lnPhi_dP)
    d_lnPhi_dP = (ln_fugacityCoef-d_lnPhi_dP)/2.d-4/P
    V = (d_lnPhi_dP + 1.d0/P)*R*T
    CALL DENSITY(phase,P,T,X,rho)

! Calculate the partial molar enthalpy

    CALL FCOEF(phase,P,T*1.0001d0,X,ln_fugacityCoef)
    CALL FCOEF(phase,P,T*0.9999d0,X,d_lnPhi_dT)
    d_lnPhi_dT = (ln_fugacityCoef-d_lnPhi_dT)/2.d-4/T
    H = -T*d_lnPhi_dT

! Calculate the partial internal energy

    U = H - P*d_lnPhi_dP

! Calculate the output

    Qnet = (-U+V*sum(X*U)/sum(X*V))/4.d0

END SUBROUTINE Qdiff

```